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DEPARTMENT OF COMMERCE AND LABOR

COAST AND GEODETIC SURVEY

O. H. TITTMANN
SUPERINTENDENT

GEODESY

FORMULÆ AND TABLES FOR THE COMPUTATION OF GEODETIC POSITIONS

(FIFTH EDITION)

WITH A PREFACE BY

CHARLES R. DUVALL
Computer, Coast and Geodetic Survey

SPECIAL PUBLICATION No. 8



WASHINGTON
GOVERNMENT PRINTING OFFICE
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FORMULÆ AND TABLES FOR THE COMPUTATION OF GEODETIC POSITIONS.

Preface by Charles R. Duvall, Computer, Coast and Geodetic Survey.

INTRODUCTORY REMARKS.

The supply being exhausted of Appendix No. 9, Coast and Geodetic Survey Report for 1894, "Formulæ and Tables for the Computation of Geodetic Positions" (fourth edition), the present edition was made necessary. Advantage was taken of this opportunity to include the extension of the tables to the equator, which was published as Appendix No. 4, report for 1901. The present tables therefore extend from the equator to latitude 72°.

In both the above publications the development of formulæ is given in considerable detail, and in the 1894 appendix there are some historical notes in regard to the different editions of the tables. It was thought advisable to omit the development of formulæ and the historical matter in the present edition and to give, instead, a general explanation of the methods followed in computing and the degree of accuracy that might be expected from the adopted formulæ and methods.

One question that called for decision before printing a new edition of these tables was whether our present knowledge of the size and shape of the earth justified any change in the reference spheroid. When the change was made in 1880 from the Bessel spheroid to the Clarke spheroid of 1866, as expressed in meters, the major axis was increased by about 1 part in 8 000 and the minor axis by about 1 part in 13 000, the newly adopted spheroid being larger and flatter. In "Supplementary Investigation in 1909 of the Figure of the Earth and Isostasy," page 77, Hayford gets values for the major and minor axes of the earth which are larger than the Clarke values of 1866 by about 1 part in 35 000 and 20 000, respectively. It is thus seen that the spheroid which most nearly fits the geoid surface in the United States is larger than the Clarke spheroid of 1866, but with a flattening lying between that of Clarke and of Bessel. The change from Clarke to Hayford is not demanded with the same force as was the change from Bessel to Clarke. Expediency weighs heavily against any change on account of the immense amount of labor involved in transforming the large number of trigonometric points already developed on the Clarke spheroid. For all questions of geography and of geodesy the Clarke spheroid answers every practical requirement. However, it is desirable in dealing with the scientific problem of the figure of the earth that with each new accession of data a new spheroid fitting the geoid with the greatest possible accuracy should be derived. It may be remarked here that European countries are still using the Bessel spheroid, though in many of these countries a better fitting spheroid

could be adopted. Besides the reasons given above for no present change in this country, the Europeans have the additional argument of the existence of extensive tables based on the Bessel spheroid, such as Albrecht's, for example.

The dimensions of the adopted spheroid, the Clarke spheroid of 1866 as expressed in meters, will be found on page 19.

Recent progress in the invention and improvement of calculating machines brings up a question as to the possibility of arranging these tables for machine computing instead of preserving the previous form for logarithmic work. Where the number of factors in a product is more than two, the only mechanical device in use at present that compares in speed with the use of logarithms is the slide rule. The best forms of this instrument in present use are limited to numbers of four or five figures, while the work for which these tables are designed generally calls for seven figures. So it again appears that modern progress has not yet reached a point where a change is required.

SOLUTION OF TRIANGLES.

The triangle on the spheroid is solved by the application of the Legendre theorem. That is, one-third of the spherical excess is subtracted from each angle of the spheroidal triangle, the resulting angles being the angles of a plane triangle whose sides are approximately equal in length to the sides of the triangle on the spheroid.

The angle at each vertex of the spheroidal triangle is the angle between the two vertical planes at that vertex passed respectively through the sea-level projection of each of the other two vertices. Reduction is thus made for elevation above the *geoid* and not above the *spheroid*, for object sighted upon. Horizontal angles and directions are not reduced for local deflection of the vertical, for horizontal refraction, or for difference of direction between vertical section and geodetic (shortest) line. Nor are bases reduced for difference of elevation between geoid and spheroid. These refinements of computation, amounting generally to less than the uncertainties of errors of observation, remain to be applied at some future time as a second approximation to the primary triangulation in the United States.

For two points, A_1 and B_1 on the spheroid, the plane which contains the normal at A_1 and passes through B_1 intersects the spheroid in a plane curve, which may be called the vertical section from A_1 to B_1 . The vertical section from B_1 to A_1 is determined by the plane which contains the normal at B_1 and passes through A_1 . These two vertical sections do not coincide, except in particular cases, so it is not strictly accurate to say that a triangle is formed on the spheroid by the vertical sections joining three points. There are eight triangles actually formed, the sides and angles of any one differing extremely little from the corresponding sides and angles of any other, for triangles that actually enter into geodetic work—that is, for triangles whose vertices are intervisible. This ambiguity is entirely independent of that arising from extending the lines.completely around the earth. The latter ambiguity does not occur in practical application to intervisible points. The fact that horizontal directions are not reduced to the direction of geodetic lines is the source of the above difficulty, but the effect on the resulting lengths is small, being well within the uncertainty due to errors of observation. The error in length due to this cause can not accumulate, since the lengths of the controlling bases do not require a corresponding correction. The effect on the azimuth is small and also well within the uncertainties arising from errors of observation.

SPHERICAL EXCESS.

The spherical excess is computed by the formula:

$$\varepsilon = \frac{a_1 b_1 \sin C_1 (1 - e^2 \sin^2 \phi)^2}{2a^2 (1 - e^2) \sin 1''} = a_1 b_1 \sin C_1 \times m$$

In this formula ε is the spherical excess; $a_1 b_1$ and C_1 are two sides and the included angle, respectively, of the corresponding triangle; e^2 is the square of the eccentricity, and a the major semiaxis of the spheroid of reference; and ϕ is the mean latitude of the three vertices of the triangle. That part of the above expression which depends only on the latitude and the dimensions of the spheroid may be designated by a single letter, m, as shown. In Table I, page 16, the logarithms of m are given with the latitude as an argument.

The above formula gives the spherical excess too small by one one-hundredth of a second for an equilateral triangle with 200-kilometer sides, or for a nonequilateral triangle of the same area. For an equilateral triangle of 100-kilometer sides, or an equivalent nonequilateral triangle, the excess as given by this formula is too small by less than one one-thousandth of a second.

In cases where a more accurate value of the spherical excess is required the formulæ given on page 51 of Special Publication No. 4 ("The Transcontinental Triangulation") may be used. These formulæ give a slightly unequal distribution of the spherical excess among the three angles of the triangle.

NUMBER OF FIGURES IN ANGLES AND LENGTHS.

According to present practice in the Coast and Geodetic Survey, directions, angles, and azimuths are computed to the hundredth of the sexagesimal second for primary triangulation and to the tenth for secondary and tertiary work. This gives from one to two uncertain figures in the corresponding values—the uncertainties due to errors of observation—and appears to be as much as can reasonably be required of the computation at the present time.

The logarithms of the lengths, expressed in meters, are given to seven decimal places for the primary lines and to six places for secondary and tertiary lines. The lengths being computed from the angles, it is best to use seven decimal places in the lengths with hundredths of seconds in the angles and six places with tenths of seconds. In reasonably well-shaped triangles this secures against the introduction of accumulated error in the last decimal place of the logarithms of the lengths due to those small accumulations in the last decimal place of the angles which arise from rounding off to the last place used. In other words, no uncertainty is introduced into the last figure of the lengths by the computing except the unavoidable accumulation due to rounding off.

An uncertainty of a unit in the fifth decimal place of the logarithm is equivalent to an uncertainty of 1 part in 43 000, while one in the sixth place corresponds to 1 part in 434 000. The base lines are scarcely more accurate than the latter ratio; so it follows at once that even for the most accurate primary triangulation the logarithms of the lengths are surely uncertain in the sixth and seventh places, and in some cases the fifth place may be uncertain by as much as a unit. Therefore it may be said that in the use of seven decimals in the logarithms for the primary lines from two to three of the

last figures are uncertain, and with the use of six decimals for secondary and tertiary lines the last two figures are uncertain.

In passing from the logarithm to the corresponding number the uncertainty in the logarithm is, in general, reproduced by the same amount in the corresponding figure of the number. For example, an uncertainty of one in the sixth decimal of the logarithm gives rise to an uncertainty of one in the sixth figure of the number. The counting is from the left to the right in the number, beginning with the first significant figure. This correspondence for figures in the same place in the logarithm and in the number is exact for numbers whose first figures are 434 For all numbers from 100 to 434 . . . the uncertainty in the derived numbers is less than the uncertainty in the corresponding figure of the logarithm, being only about one-fourth as much for the former numbers. From 434 to 999 the uncertainty in the derived numbers is greater than the uncertainty in the corresponding figure of the logarithm, being about two and one-half times as great in the latter numbers. On the whole, then, the numbers should be written out to as many significant figures as there are decimal places in the logarithms from which they are derived, and the uncertainties will be about the same for corresponding figures. If this rule were followed out, it could always be said that there were two uncertain figures in the given lengths. The length of the lines varies between such wide limits, however, that the application of such a rule would give a nonuniform appearance to the results, so the practice in the Coast and Geodetic Survey is to give the lengths to two decimal places (centimeters) for the primary lines and to one decimal place for the secondary and tertiary lines.

COMPUTATION OF DIFFERENCES OF LATITUDE, LONGITUDE, AND AZIMUTH.

The problem is, given the latitude and longitude of a point A_1 and the azimuth and distance from A_1 to B_1 , to determine the latitude and longitude of B_1 and the azimuth from B_1 to A_1 . The distance here used is the side of a triangle, computed as explained above, and the azimuth is the angle the vertical section makes with the meridian, measured clockwise from the south up to 360°. The meridian referred to is not the directly observed meridian, but is one carried to the point in question through the triangulation and is, in general, based on many directly observed astronomic azimuths. It is customary in the Coast and Geodetic Survey to speak of this azimuth as the geodetic azimuth, meaning the azimuth of the vertical section as carried through the triangulation and having no reference to the azimuth of the geodetic (shortest) line. The formulæ used in the solution of the above problem are as follows:

(1)
$$- \varDelta \phi = s \cos \alpha \cdot B + s^2 \sin^2 \alpha \cdot C + (\delta \phi)^2 D - h \ s^2 \sin^2 \alpha \cdot E - 1/2 \ s^2 k E + 3/2 \ s^2 \cos^2 \alpha \cdot k E + 1/2 \ s^2 \cos^2 \alpha \sec^2 \phi \ A'^2 k \sin^2 1'';$$

(2)
$$\sin \Delta \lambda = \sin \frac{s}{N'} \sec \phi' \sin \alpha;$$

or

or
$$\log J\lambda = \log s + C_{\log J\lambda} - C_{\log s} + \log \sin \alpha + \log A' + \log \sec \phi';$$

(3)
$$-\tan \frac{1}{2} (J\alpha) = \tan \frac{1}{2} (J\lambda) \frac{\sin \frac{1}{2} (\phi' + \phi)}{\cos \frac{1}{2} (\phi' - \phi)};$$

 $-J\alpha = J\lambda \sin \frac{1}{2} (\phi' + \phi) \sec \frac{1}{2} (J\phi) + (J\lambda)^3 F.$

In (1) the following abbreviations are made:

$$h = s \cos \alpha \cdot B;$$

$$-\delta \phi = s \cos \alpha \cdot B + s^2 \sin^2 \alpha \cdot C - h \ s^2 \sin^2 \alpha \cdot E;$$

$$k = s^2 \sin^2 \alpha \cdot C.$$

The symbols in the above expressions are as follows: ϕ and λ are the given latitude and longitude, respectively, of the point A_1 ; ϕ' and λ' represent the required latitude and longitude, respectively, of the point B_1 ; s is the distance from A_1 to B_1 ; α is the azimuth of the vertical section from A_1 to B_1 , and α' is the azimuth of the vertical section from B_1 to A_1 ; N' is the length of the normal at the point B_1 . The differences of latitude, longitude, and azimuth are represented, respectively, by $\Delta \phi$, $\Delta \lambda$, and $\Delta \alpha$, and—

$$\phi' = \phi + \Delta \phi;$$

$$\lambda' = \lambda + \Delta \lambda;$$

$$\alpha' = \alpha + \Delta \alpha + 180^{\circ};$$

A', B, C, D, E, and F are factors depending on the dimensions of the reference spheroid and the latitude. The forms of these factors are shown on page 19, and their logarithms are given with the latitude as an argument in Table V.

Equation (1) gives the difference of latitude in the form of a power series of the distance. Although terms of the sixth order appear in this expression, it can not be said to be correct up to terms of the fourth order. This formula is limited in application both by latitude and by length of line. Latitudes near 90° are excluded since the tangent of the latitude enters into some of the coefficients. For a required degree of accuracy in $J\phi$ —for example, that the third decimal place of the seconds shall be correct, according to usage in the Coast and Geodetic Survey—the length of line to which (1) is applicable is limited accordingly. In Appendix No. 7, Coast and Geodetic Survey Report for 1896, page 303, it is stated that (1) and (2) should not be applied to lines of greater length than 75 kilometers if the results are required to be correct to 0".oor. When this statement was made the terms of the fourth order were not included in (1), and the statement seems to have allowed considerable margin for safety.

Equation (2) gives $\Delta \lambda$ by the solution of a spherical triangle. In passing to the second form, which is more convenient for computing, corrections are given for the second term in the reduction from the logarithm of the sine to the logarithm of the arc.

The form of this correction for $\Delta\lambda$ is $\frac{M}{6}\sin^2 \pi''(\Delta\lambda)^2$, in which M is the modulus of the

common system of logarithms, and $\Delta \lambda$ is expressed in seconds; the form for s is $\frac{M}{6}s^2$ A'^2 $\sin^2 I''$, in which s is in meters and A' is the factor given in (2). This factor is written with the prime accent to emphasize the fact that in the use of (2) it is to be taken from the tables for the latitude ϕ' and not ϕ . In Table II the exact correction to the logarithm of $\Delta \lambda$ is placed in the middle, while just opposite on the right is the corresponding logarithm of s to three decimal places, and opposite on the left is the corresponding logarithm of s to three places. The correction for s is always positive and that for s is always negative. In tabulating the correction for s an average value (8.509) was taken for s to the correction can not be in error on this account as

much as one in the seventh place for any latitude from 0° to 72°, as long as the line does not exceed 100 kilometers in length. In forming length equations in triangulation adjustment the correction for reduction from arc to sine is taken from Table II for log s and is, of course, always negative in this case.

Formulæ (1) and (2) do not give results correct to 0".001 in $\Delta\phi$ and $\Delta\lambda$ for lines approaching 100 kilometers in length or greater. Nevertheless the error is not more than two or three in the third decimal of the seconds for lines up to about 120 kilometers, and in general the errors due to the limitations of the formulæ are not greater for these lengths than the uncertainty arising from the use of only seven decimal places in the computations.

Formula (3) is the application of Dalby's theorem. There can be no question of the accuracy of the second decimal place of the seconds in $\Delta \alpha$, derived by the use of this formula, for any length of line for which (1) and (2) give results approximately correct to 0''.001. In passing to the second form of (3) account is taken of the second term in the expansion of $\tan \frac{1}{2}\Delta \alpha$ and $\tan \frac{1}{2}\Delta \lambda$, and an approximate value of the ratio of $\Delta \alpha$ to $\Delta \lambda$ is taken to derive the form of the factor F.

The formulæ (1), (2), and (3) are all arranged to give the results in seconds. An example is given on page 12 of the application to primary lines. The differences of latitude, longitude, and azimuth are computed for the two sides of a triangle, the base points of which are already known in latitude, longitude, distance, and mutual azimuths The solution is also shown of the triangle upon which this example is based. The practice is to write the name of the new point first in the form for the computation of triangles, the known base points following in clockwise order. The two position computations from the two known extremities of the base to the as yet unknown position of the vertex of the triangle are made on two pages which face each other. The angle opposite the second name in the triangle computation is always entered on the left-hand page and is added to get the resulting azimuth from that point to the vertex. The third angle is placed on the right-hand page and always subtracted to get the resulting azimuth from the other base point. This rule of always writing the names and angles of the triangle in clockwise order and entering the angles and adding and subtracting in a specified way on the position computation forms is mechanical, but is conducive to accuracy and speed in computing. The latitude and longitude of the vertex of the triangle both appear on opposite pages, and an immediate check is furnished, while the two azimuths from the vertex back to the base points are checked if the azimuth on the right-hand page is equal to the sum of the azimuth on the left-hand page and the first angle of the triangle (called third angle in the 1911 edition of the position computation forms, which were used in the following sample computations).

In the examples given below, what is printed on the forms is indicated by roman type and italics, while the part filled in for the special computation is shown in bold-face type. No printed form is used for computing spherical excess, as it is a simple matter to add the logarithm from Table I to the three logarithms in the triangle computation, a preliminary computation of the triangle being sufficiently accurate for this purpose.

To apply these tables to the computation of positions south of the equator it is only necessary to bear in mind in using the formulæ that all south latitudes are negative. Wherever $\Delta \phi$, as computed in these formulæ, is negative, it indicates a numerical

increase in the latitude. In using the formulæ for $J\alpha$ it should be noted that for the Southern Hemisphere the term $\sin \frac{1}{2}(\phi + \phi')$ is always negative, and therefore $J\alpha$ and $J\lambda$ always have the same sign in the Southern Hemisphere, whereas they have opposite signs in the Northern Hemisphere.

To apply these tables to the computation of positions in east longitude it is only necessary to consider that all east longitudes are negative.

In the logarithms given in the tables a minus sign over the characteristic indicates that 10 is to be subtracted from the characteristic as printed, and a double minus sign indicates that 20 is to be subtracted from the characteristic as printed.

EXAMPLES OF COMPUTATION.

Computation of triangles.

No.	Stations.	Obse	rved	angles.	Correction.	Spherical angles.	Spher- ical excess.	Plane angles.	Logarithms.
1 2 3	Marysville Butte to Kent Lyons Marysville Butte Kent Lyons to Kent Lyons to Marysville Butte	61 49 68	23 55 41	36.35 13.85 37.45	+0.43 03 54	36.78 13.82 36.91	9.17 9.17 9.17 9.17	27.61 04.65 27.74	5.062 7330 0.056 5511 9.883 7314 9.969 2455 5.003 0155 5.088 5296

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Position computation, primary triangulation.

α	K	arysville Butte ent arysville Butte	& Lyons				_	137 + 49 187 +	16 55 11 6	13.82
α'	ı. Ly	ons ,	to 2. Marys	ville Butte	Third	angle of	triangle	180 7 61	18 23	50.85 36.78
φ Δφ φ'	39	9 12 22.361 1 05 43.740	2. Marysv	ille Butte			λ Δλ λ'	121 -	/ 49 10 38	11.540 50.533 21.007
$cos \alpha B$	8	5.088 5296 0.996 5633 <i>n</i> 3.510 9119 3.596 0048 <i>n</i>	$\sin^2 \alpha$ C	0.17706 8.19596 1.31615 9.68917	$(\hat{\delta}\phi)^2$ D	7.1918 2.3833 9.5751	$ \begin{array}{c c} -h \\ s^2 \sin^2 \alpha \\ E \end{array} $	r	8.3 6.0	960 730 878
ıst t		-3 944.6164 + .4888	3d term 4th term	+0.3760 + .0114			F $(J\lambda)^3$		8.4	71
3d and term	ms 1ϕ	+ .3874 -3 943.7402 -3 943.7402 39 45 14.23	$ \begin{array}{ccc} s & s \\ \sin \alpha & A' \\ sec \phi' \end{array} $	5.088 5296 9.097 9799 <i>n</i> 8.509 1108 0.117 6752	Arg.	$-268 \\ + 7$	Δλ sin ½(φ+ sec ½(Δς	φ') b)	9.8	13 269 <i>n</i> 05 835 00 020
			Δλ	-261 2.813 2694 <i>n</i> -650.5330	Corr.	-261	-Jα			19 124 <i>n</i> // 16.030 .000

Position computation, primary triangulation.

α Δ Δ Δα	Ly	ent to Mary ons & Mary ent to 1. Lyons	sville Butte sville Butte		•			310 - 68 - 24' +	8 41 36.91
α'	ı. Ly	ons to 3. Kent						186 6	
φ 1φ	39		3. Kent				λ 1λ	° 122 — 1	
φ'	40	18 06.101	1. Lyons				λ.	121	38 21.007
s $\cos \alpha$ B	g	5.003 0155 0.573 5793 <i>n</i> 3.510 8543	$\sin^2 \alpha C$	0.00603 9.93433 1.32783	$(\partial \phi)^2 D$	6.1615 2.3856	$ \begin{array}{c c} -h \\ s^2 \sin^2 \epsilon \\ E \end{array} $	α	3.0874 9.9404 6.1036
	term term	3.087 4491n $-1 223.0637$ $+ 18.5434$	3d term 4th term	1.26819 // +0.0353 +0.1353		8.5471	F $(J\lambda)^3$	3	9.1314 0.791 7.869
ter –	ad 4th rms	$ \begin{array}{r} -1 & 204.5203 \\ + & .1706 \\ \hline -1 & 204.3497 \\ \circ & ' & '' \\ 40 & 08 & 03.93 \end{array} $	$ \begin{array}{c} s \\ \sin \alpha \\ A' \\ \sec \phi' \end{array} $	5.003 0155 9.967 1652 <i>n</i> 8.509 1108 0.117 6752	Arg. s Δλ	$-180 \\ +267$	Δλ sin ½(φ+ sec ½(Δ		3.596 975 <i>n</i> 9.809 279 0.000 002
/2(Ф	+\$\psi')	40 00 03.93	٦)	+87 3.596 9754 <i>n</i> -3 953.4423	Corr.	+ 87		{	3.406 256 <i>n</i> -2 548.3305

For subordinate triangulation when the sides do not exceed, say, 25 kilometers, or about 15 miles, the term involving E in $\mathcal{I}\phi$ and the factor sec $\mathcal{I}_2\mathcal{I}\phi$, as well as the term involving F in $\mathcal{I}\alpha$, may be omitted. The number of decimal places used in computing the small terms of $\mathcal{I}\phi$ may be reduced for this class of triangulation, as is shown in the example given below. Only one side of the double computation is shown in this case, though in practice the computation is always made for the two sides of the triangle in order to have complete checks.

Position computation, secondary triangulation.

α Δ α Δα	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	43 54.0 46 17.3 30 11.3 1 54.7 00 00.0 28 16.6							
	28	35 02.377 2 36.805	λ Δλ	96 +	26 59.604 3 59.900				
ıst t 2d ar ter	erm id 3d ms	28 33 44 // +156.7458 + .0594	$\cos \alpha$ B	9.77	74 355 11 666	sin ²	9.81 1.14 8.77	$\frac{h^2}{h^2}$	6.71
		$\sin \alpha \ A'$	9.905 8.509 0.056	196 391 268 030		+\$\phi'\$)	9.67953 2.05956	5	

The inverse problem.—Cases frequently occur where the distance and mutual azimuths are demanded for two points whose latitudes and longitudes only are known. It has not been found necessary to prepare special formulæ and blank forms for this computation, as it can be readily made with the help of the preceding forms. It is done by dividing $\Delta \lambda = s \sin \alpha \cdot A' \sec \phi'$ by the first term for $\Delta \phi$, $h = s \cos \alpha \cdot B$, whence we get—

$$\tan \alpha = \frac{\Delta \lambda B}{A' \sec \phi' h}$$

This would give the azimuth at once, provided we knew h, since $\Delta \lambda$ is given. We therefore compute the smaller terms for the difference of latitude in order to obtain h by

subtracting them from the known value of $J\phi$. The only addition to the usual form is the term $\log \tan \alpha = \log (s \sin \alpha) - \log (s \cos \alpha)$. The value of s will best be taken from the term h when $\sin \alpha$ exceeds $\cos \alpha$, and from the term $J\lambda$ when the reverse is the case. When the distance s is large, as in primary triangulation, it will be necessary to introduce the correction for $J\lambda$ due to difference of ratio between sine and arc, using inversely the form for primary work.

The accuracy with which the length and azimuth can be derived from the given positions of the two points depends on the number of decimal places to which the seconds of the latitudes and longitudes are given, as well as on the length of the line. If the latitudes and longitudes are given to the third decimal place of the seconds, the length can be determined to within about 5 centimeters for any length of line to which the formulæ are applicable. The accuracy with which the azimuth is determined depends on the length of line, being more accurate for the longer lines.

Position computation, secondary triangulation.

INVERSE SOLUTION.

α		to					0	,	"
		&					+		
α	2 Sand	Point to 1	Indianola				53	30	
α'	1 Indian	nola to 2	Sand Poin		ird angle of	triangle	180 233		
φ L	28 3	, ,, 5 02.377 2 36.805	2 Sand I	Point		λ	96 +	26 3	59.604 59.900
φ'	28 3	2 25.572	1 Indian	ola		λ'	96	30	59.504
rst 2d a te	term - and 3d - rms	8 33 44 1156.7455 1 .0595 1 .0595	$cos \alpha B$	3.683 529 8.511 666 2.195 195	$\sin^2 \alpha$	7.6287 1.1419 8.7706 .0590	h^2		4.39 2.32 6.71 .0005
	$\sin \alpha$ A' $\sec \phi'$			$^{J\lambda}$ $\sin \frac{1}{2}(\phi+\phi')$	2.380 (9.679 \ 2.059 \	s co tar co	$\alpha = 3.$ $\alpha = 3.$ $\alpha = 0.$ $\alpha = 53$ $\alpha = 9.$ $s = 3.$	683 130 30 1	529 842
1	Δλ	1	9.900	-1α	+114	.7			

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I. Table of log m.

Lat.	log m.	Lat.	log m.	Lat.	log m.	Lat.	log m.
o oo o	ī. 40695 695 695 694 694	0 00 20 30 21 00 21 30 22 00	ī. 40626 623 619 616 612	0 / 40 00 40 30 41 00 41 30 42 00	ī. 40452 446 441 436 431	60 00 60 30 61 00 61 30 62 00	ī. 40253 249 244 240 235
2 30 3 00 3 30 4 00 4 30	694 693 693 692 691	22 30 23 00 23 30 24 00 24 30	608 605 601 597 594	42 30 43 00 43 30 44 00 44 30	426 421 416 411 406	62 30 63 00 63 30 64 00 64 30	231 227 223 219 215
5 00 5 30 6 00 6 30 7 00	690 689 688 687 686	25 00 25 30 26 00 26 30 27 00	590 586 582 578 573	45 00 45 30 46 00 46 30 47 00	400 395 390 385 380	65 00 65 30 66 00 66 30 67 00	210 207 203 199
7 30 8 00 8 30 9 00 9 30	685 683 682 680 679	27 30 28 00 28 30 29 00 29 30	569 565 560 556 552	47 30 48 00 48 30 49 00 49 30	375 369 364 359 354	67 30 68 00 68 30 69 00 69 30	192 188 185 181 178
10 00 10 30 11 00 11 30 12 00	677 675 673 671 669	30 00 . 30 30 31 00 31 30 32 00	548 544 539 534 530	50 00 50 30 51 00 51 30 52 00	349 344 339 334 329	70 00 70 30 •71 00 71 30 72 00	174 171 168 164 T. 40161
12 30 13 00 13 30 14 00 14 30	667 665 663 660 • 658	32 30 33 00 33 30 34 00 34 30	525 520 516 511 506	52 30 53 00 53 30 54 00 54 30	324 319 314 309 304		
15 00 15 30 16 00 16 30 17 00 *	655 653 650 647 644	35 00 35 30 36 00 36 30 37 00	501 496 491 486 482	55 00 55 30 56 00 56 30 57 00	299 295 290 285 280		
17 30 18 00 18 30 19 00 19 30	642 639 636 632 7. 40629	37 30 38 00 38 30 39 00 39 30	477 472 467 462 1. 40457	57 30 58 00 58 30 59 00 59 30	276 271 266 262 1. 40257		

[The above table is computed for the Clarke spheroid of 1866 as expressed in meters.]

II.—Table of corrections to log $\Delta\lambda$ for difference in arc and sine.

$\log s(-)$ log difference. $\log J\lambda(+)$	log s (-) log difference.	log J $\lambda(+)$	log s (-) log differe	ence. $\log J\lambda(+)$
3.876 0.000 0001 2.385	4. 871 0. 000 0098		5. 172 0. 000 0	
4. 026 02 2. 535	4. 882 103		5. 178	402 3.687
4. 114 03 2. 623	4. 892 108	-	5. 183 5. 188	412 3.692
4. 177 04 2. 686	4. 903		•	422 3.697
4. 225 05 2. 734	4. 913	3. 422	5. 193	433 3.702
4. 265 06 2. 774	4. 922 124	0 .0	5. 199	443 3. 708
4. 298 07 2. 807	4. 932		5. 204	453 3.713
4. 327 08 2. 836	4. 941 136		5. 209	464 3.718
4. 353 09 2. 862	4. 950 142		5. 214	47,4 3. 723
4. 376 10 2. 885	4. 959	3. 468	5. 219	486 3.728
4. 396 11 2. 905	4. 968	3. 477	5. 223	497 3.732
4. 415 12 2. 924	4. 976	0 ' 0	5. 228	508 3.737
4. 433 13 2. 942	4. 985	3. 494	5. 233	519 3.742
4. 449 14 2. 958	4. 993	3. 502	5. 238	530 3.747
4. 464 15 2. 973	5. 002 179	3. 511	5. 242	541 3.751
4. 478 16 2. 987	5. 010 180	3. 519	5. 247	553 3.756
4. 491 17 3. 000	5. 017 192	0 0 /	5. 251	565 3.760
4. 503 18 3. 012	5. 025 199		5. 256	577 3.765
4. 526 20 3. 035	5. 033 200		5. 260	588 3.769
4. 548 23 3. 057	5. 040 213		5. 265	600 3. 774
4. 570 25 3. 079	5. 047 22	3. 556	5. 269	613 3.778
4. 591 27 3. 100	5. 054 228		5. 273	625 3. 782
4. 612 30 3. 121	5. 062 230		5. 278	637 3. 787
4. 631 33 3. 140	5. 068 24		5. 282	650 3.791
4. 649 36 3. 158	5. 075 25		5. 286	663 3.795
4. 667 39 3. 176	5. 082 250	3. 591	5. 290	674 3. 799
4. 684 42 3. 193	5. 088 26		5. 294	687 3.803
4. 701 45 3. 210	5. 095 27.		5. 299	702 3.808
4. 716 48 3. 225	5. 102 28		5. 303	716 3.812
4. 732 52 3. 241	5. 108 29		5. 307	729 3.816
4. 746 56 3. 255	5. 114 30	3. 623	5. 311	743 3.820
4. 761 59 3. 270	5. 120 30		5. 315	757 3.824
4. 774 63 3. 283	5. 126	3.635	5. 319	771 3.828
4. 788 67 3. 297	5. 132		5. 323	785 3.832
4. 801 71 3. 310	5. 138 33		5. 327	800 3.836
4. 813 75 3. 322	5. 144 34	5 3.653	5. 331	814 3.840
			5. 335	829 3.844
	5. 150 5. 156 35		5. 339	845 3.848
4. 834 4. 849 89 3. 358	5. 161 37		5. 343	861 3.852
	5. 167 38		5· 343 5· 347	877 3.856
4. 860 94 3. 369	5. 10/	3.070	3. 241	5// 5/050

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III.—Table of values of log sec $\frac{1}{2}$ (2ϕ) .

Дф	log sec ½ (Δφ)	$\mathcal{A}\phi$	log sec ½ (Δφ)	Jφ	log sec ½ (Δφ)	Δφ	log sec ½ (Δφ)	10	log sec ½ (J φ)
,		,		,		,		,	
10	0. 000 000	28	0.000 004	46	0.000 010	64	0. 000 019	82	0.000 031
II	I	29	4	47	10	65	19	83	32
12	I	30	4	48	II	66	20	84	32
13	I	31	4 [49	II	67	21	85	33
14	I	32	5	50	II	68	21	86	34
15	ı	33	_	51	12	69	22	87	35
16	ī	34	5 5 6 6	52	12	70	22	88	35 36
17	I	35	ě	53	13	71	23	89	36
18	I	36		54	13	72	24	90	37 38
19	2	37	6	55	14	73	24	91	38
20	2	38	7	56	14	74	25	92	39
2 I	2	39	7	57	15	75	26	93	40
22	2	40	7 8 8	58	15	76	26	94	41
23	2	41	8	59	16	77	27	95	41
24	3	42	8	60	16	78	28	96	42
25	3	43	8	61	17	79	29	97	43
26	3	44	9	62	18	80	29	98	44
27	3 3	45	9	63	18	81	30	99	45

For the convenience of the computer the following conversion table is inserted:

IV.—Conversion table.

То со	nvert;	To convert:					
Meters to feet.	Feet to meters.	Kilometers to statute miles.	Statute miles to kilometers.				
1= 3. 280 833 2	1=0.304 8006 2 0.609 6012 3 0.914 4018 4 1.219 2024 5 1.524 0030 6 1.828 8037 7 2.133 6043 8 2.438 4049 9 2.743 2055	1=0. 621 3699 2	1= 1.609 347 2 3.218 694 3 4.828 042 4 6.437 389 5 8.046 736 6 9.656 083 7 11.265 430 8 12.874 778 9 14.484 125				

V.—Table of logarithms of factors A', B, C, D, E, F, based upon the Clarke spheroid of 1866 as expressed in meters, between latitudes 0° and 72°.

CONSTANTS.

	Equatorial semi-axis= a Polar semi-axis= b	6 356 583.8	
	b/a=	293. 98 294. 98	
$A' = \frac{(1 - e^2 \sin^2 a \sin a)}{a \sin a}$	$\phi')^{\frac{1}{2}}$	lo	g $a=6.804$ 698 57 g $b=6.803$ 223 78 g $e^2=\overline{7}.830$ 502 57
$B = \frac{(1 - e^2 \sin^2 \alpha)}{a(1 - e^2) \sin^2 \alpha}$		_	$\frac{1}{1''} = 8.50972656$ $\frac{1}{1''} = 8.51267615$
$C = \frac{(1 - e^2 \sin^2 \theta)}{2a^2 (1 - e^2)}$ $D = \frac{\frac{3}{2}e^2 \sin \phi}{1 - e^2}$		$\log \frac{1}{2a^2 (1-e^2) \sin}$	
	$\frac{\phi)\left(1-e^2\sin^2\phi\right)}{6a^2}$	log	$\frac{1}{6a^2} = \overline{5}.612 \ 45$ $1'') = \overline{8}.291 \ 96$

LATITUDE o'.

Lat.	log A'	log B	log C	log D	log E	log F
° ', 00 00 I	8. 509 7266 66 66	8. 512 6761 61 61	-∞ 7.8707	-∞ -∞ 	\(\frac{1}{5} \). 6125	-∞
3 4	66 66	61 61	. 1717 3477 4727	457 633 758	5 5 5	
°5 6 7 8	66 66 66 66 66	61 61 61 61 61	5696 6488 7158 7740 8249	855 9 . 934 0 . 001 0 59 110	5 5 5 5 5	
10 11 12 13 14	8. 509 7266 65 65 65 65	8. 512 6761 61 61 61 61 61	8. 8707 9121 9499 8. 9846 9. 0168	o. 156 197 235 270 302	5. 6125 5 5 5 5	
15 16 17 18	65 65 65 65 65	61 61 60 60 60	0468 0748 1011 1259 1494	332 360 386 411 435	5 5 5 5 5	
20 21 22 23 24	8. 509 7265 65 65 65 65	8. 512 6760 60 60 60 59	9. 1717 1929 2131 . 2324 2509	0. 457 478 498 518 536	5. 6125 5 5 5 5	₹. 057
25 26 27 28 29	65 65 65 65 65	59 59 59 59 58 .	2686 2857 3020 3178 3331	554 571 587 603 618	5 5 5 5 5	
30 31 32 33 34	8. 509 7265 64 64 64 64	8. 512 6758 58 58 57 57	9. 3478 3620 3758 9. 3892 9. 4022	0. 633 647 661 674 687	5. 6126 6 6 6 6	
35 36 37 38 39	64 64 64 64 64	57 57 56 56 56	4148 4270 4389 4505 4618	700 712 724 736 747	6 6 6 6	
40 41 42 43 44	8. 509 7264 64 64 64 63	8. 512 6756 55 55 55 55 54	9. 4728 4835 9. 4939 9. 5042 5141	0. 758 769 779 789 799	5. 6126 6 6 6 7	6. 358
45 46 47 48 49	63 63 63 63 63	54 54 53 53 53	5239 5335 5428 5519 5609	809 819 828 837 6 46	7 7 7 7 7	
50 51 52 53 54	8. 509 7263 63 62 62 62	8. 512 6752 52 51 51 51	9. 5697 5783 5866 9. 5950 9. 6031	o. 855 863 872 880 888	5. 6127 7 7 7 7 8	
55 56 57 58 59	62 62 62 61 61	50 50 49 49 49	6111 6189 6266 6341 6416	896 904 912 919 927	8 8 8 8	
60	8. 509 7261	8. 512 6748	9. 6489	0. 934	5. 6128	6. 534

LATITUDE 1°.

° , I 00 I 2 3 4	8. 509 7261 61		,			
1 2 3					_	=
3	6-	8. 512 6748	5. 6489	ō. 934	<u>5</u> . 6128	6 . 534
.3		48	560	941	29	
.3	61	47	631	948	29	
4	61	47	701	955	29	
	61	46	769	962	29	
o ₅	60	• 46	836	969	29	
0	60	45	903	975	29	
7 8	60	45	9. 6968	982	29	
	60 60	44	9. 7032 096	988	30	•
9		-14	090	0. 995	30	
10	8. 509 7260	8. 512 6743	9. 7158	1.001	5. 6130	
II	59	43	220	007	30	
12	59	42	281	013	30	
13	59	42	341	019	30	
14	59	41	400	025	31	
15	59	41	458	031	31	
16	58	40	516	037	31	
17 18	58	39	572	042	31	
	59 58 58 58 58	39	628 684	048	31	
19	58	38	684	o 53	31	
20	8. 509 7258	8. 512 6738	9. 7738	1. 059	5. 6132	6. 658
2 I	57	37	792	064	32	
22	57	36	846	070	32	
23	57	36	898	0 75	32	
24	57	35	9. 7950	080	32	
25	57	35	9. 8002	085	32	
26	56	34	053	090	33	
27	56	33	103	095	33	
28	• 56	33	152	100	33	
29	56	32	202	105	33	
30	8. 509 7256	8. 512 6731	9. 8250	1. 110	5. 6133	
31	55	31	298	115	34	
32	55	30	346	119	34	
33	55 55	29	393	124	34	
34	55	29	439	129	34	
35	54	28	485	133	34	
36	54	27	531	138	35	
37	54	26	576	142	35	
38	54	26 35	620 664	147 151	35	
39	53	25		-31	35	
40	8. 509 7253	8. 512 6724	9. 8708	1. 156	5. 6136	6. 755
41	53	23	751	160	36 36	
42	53	23	794	164 -69	30	
43	52	22	836 878	168	36 36	
44	52	21	878	173	36	
45	52	20	920	· 177	37	
46	52	20	9. 8961	181	37	
47 48	51	19 18	9. 9002	185 189	37	
	51		042 082	193	37 38	
49	51	17	002	*93		
50	8. 509 7251	8. 512 6716	9.9122	1. 197	5. 6138	
51	50	16	161	201	38 38	
52	50	15	200	205	38	
53	50	14	239	209	39	
54	49	13	277	212	39	
55	49	12	315	216	39	
55 56	49	II	353	220	39	
57 58	49 48	10	390	224	40	
58	48	10	427	227	40	
59	48	09	464	231	40	
60	8, 500, 7248	8. 512 6708	9. 9500	1. 2347	5. 6140	6. 834

COAST AND GEODETIC SURVEY.

LATITUDE 2°.

Lat.	log A'	log B	log C	log D	log E	log F
° ' 2 00 I 2 3 4	8. 509 7248 47 47 47 47	8. 512 6708 07 06 05 04	5. 95002 5363 5721 6076 6428	ī. 2347 383 419 454 489	5. 6140 41 41 41 41	ē. 8 ₃₄
o5 6 7 8 9	46 46 46 45 45	03 02 01 6700 6699	6777 7123 7467 78 0 8 8146	524 559 593 627 661	42 42 42 43 43	
10 11 12 13 14	8. 509 7245 44 44 44 43	8. 512 6698 97 97 96 95	9. 98482 8815 9145 9473 9. 99799	1. 2694 727 760 793 826	5. 6143 43 44 44 44	
15 16 17 18	43 43 42 42 42	94 93 91 90 89	ō. 00122 0443 0762 1078 1392	858 890 922 953 1. 2984	45 45 45 45 46	
20 21 22 23 24	8. 509 7241 41 41 40 40	8. 512 6688 87 86 85 84	o. o1703 2013 2320 2625 2928	1. 3015 046 077 107 138	5. 6146 46 47 47 47	6. 901
25 26 27 28 29	40 39 39 38 38 38	83 82 81 80 79	3229 3528 3825 4119 4412	168 197 227 256 285	48 48 48 49 °	
30 31 32 33 34	8. 509 7238 37 37 37 36	8. 512 6678 . 76 . 75 . 74 . 73	0. 04703 4992 5279 5564 5847	1. 33 ¹ 4 343 37 ² 400 428	5. 6149 50 50 50 50	
35 36 37 38 39	36 35 35 35 35 34	72 71 70 68 67	6129 6408 6686 6962 7237	456 484 512 539 567	51 51 52 52 52	
40 41 42 43 44	8. 509 7234 33 33 33 33 32	8. 512 6666 65 64 62 61	o. o7509 7780 8050 8317 8583	1. 3594 621 648 674 701	5. 6153 53 53 54 54	6. 959
45 46 47 48 49	32 31 31 31 30	59 58 56 55	8848 9111 9372 9631 0. 09890	727 753 779 8 0 5 831	54 55 55 56 56	
50 51 52 53 54	8. 509 7230 29 29 28 28	8. 512 6654 52 51 50 49	0. 10146 0401 0655 0907 1158	1. 3856 882 907 932 957	5. 6156 57 57 57 57 58	
55 56 57 58 59	28 27 27 26 26	47 46 45 43 42	1407 1655 1902 2147 2390	1. 3982 1. 4007 031 055 080	58 59 59 59 60	
60	8. 509 7225	8. 512 6641	0. 12633	1.4104	5. 6160	7. 010

LATITUDE 3°.

Lat.	log A'	$ \frac{\log B}{\text{diff. } i'' = -0.03} $	log C	log D	log E	log F
° ' 3 00 I 2 3 4	25 24 24 24	8. 512 6641 39 38 37 35	5. 12633 2874 3113 3352 3589	7. 410.4 28 52 75 1. 4199	5. 6160 61 61 61 62	7. 010
05 6 7 8 9	23 23 22 22 21	34 33 31 30 28	3825 4059 4293 4525 4756	1. 4222 46 69 1. 4292 1. 4315	62 62 63 63 64	
10 11 12 13 14	8. 509 7221 20 20 19	8. 512 6627 26 24 23 21	0. 4985 5214 5441 5667 5892	1. 4338 60 . 1. 4383 1. 4405 28	64 ' 65 65 65 66	
15 16 17 18	18 18 17 17	20 18 17 15	6116 6338 6560 6780 6999	50 72 1. 4494 1. 4516 38	66 67 67 68 68	
20 21 22 23 24	8. 509 7216 15 15 14 14	8. 512 6612 11 09 08 06	o. 17217 7434, 7650 7665 8079	1. 4560 1. 4581 1. 4603 24 45	5. 6168 69 69 70 70	7. 055
25 26 27 28 29	13 13 12 12	05 03 02 6600 6599	8292 8504 8715 8925 9133	66 1. 4687 1. 4708 29 50	71 71 72 72 72	
30 31 32 33 34		8. 512 6597 96 94 92 91	0. 19341 9548 9754 19959 20163	1. 4770 1. 4791 1. 4811 32 52	5. 6173 73 74 74 75	
35 36 37 38 39	08 08 07 07 06	86 84	0366 0568 0769 0969 1168	72 1. 4892 1. 4912 32 52	75 76 76 77 77	
40 41 42 43 44	8. 509 7206 05 04 04 03	80 78 76	0. 21367 1564 1761 1956 2151	1. 4971 1. 4991 1. 5011 30 49	5. 6178 78 79 79 80	7. 096
45 46 47 48 49	03 02 02 01 01	71 69 68	2345 2538 2731 2922 3113	68 1. 5088 1. 5107 26 45	80 81 81 81 82	
50 51 52 53 54	8. 509 7200 7199 99 98 98	63 61 59	0. 23302 3491 3680 3867 4053	1. 5163 1. 5182 1. 5201 19	5. 6182 83 84 84 85	
55 56 57 58 59	97 96 96 95 95	56 54 52 50	4239 4424 4608 4792 4974	56 75 1. 5293 1. 5311 29	85 86 86 87 87	
60	8. 500 7104	8. 512 6547	0. 25156	1. 5347	5. 6188	7- 133

LATITUDE 4°.

Lat.	log A'	log B diff. 1"=-0.04	log C	log D	log E	log F
3 4 05 6 7 8	8. 509 7194 93 93 92 92 91 91 90 89	8. 512 6547 45 43 42 40 38 36 34	ō. 25156 5337 5518 5697 5876 6055 6232 6409	T. 5347 65 1. 5383 1. 5401 18 36 54 71	5. 6188 88 89 89 90 90	7. 133
9	89	32 31	6585 6760	1. 5489 1. 5506	92 92	
10	8. 509 ,7188	8. 512 6529	o. 26935	1. 5523	5. 6193	
11	87	27	7109	40	93	
12	87	25	7282	58	94	
13	86	23	7455	75	95	
14	86	21	7627	1. 5592	95	
15 16 17 18	85 84 84 83 82	19 17 16 14 12	7798 7968 8138 8308 8476	1. 5609 25 42 59 76	96 96 97 97 98	
20 21 22 23 24	8. 509 7182 81 80 80 79	8. 512 6510 08 06 04 02	o. 28644 , 8812 8978 9144 9310	1. 5692 1. 5709 25 42 58	5. 6199 5. 6199 5. 6200 00	7. 168
25	78	6500	9475	74	01	
26	78	6498	9639	1. 5791	02	
27	77	96	9802	1. 5807	03	
28	76	*94	0. 29965	23	03	
29	76	92	0. 30128	39	04	
30	8. 509 7175	8. 512 6490	5. 30290	1. 5855	5. 6204	
31	74	88	0451	71	05	
32	74	86	0611	1. 5887	05	
33	73	84	0771	1. 5902	06	
34	72	82	0931	18	07	
35	72	80	1090	34	07	
36	71	78	1248	50	08	
37	70	76	1406	65	08	
38	70	74	1563	81	09	
39	69	72	1719	1. 5996	10	
40	8. 509 7168	8. 512 6470	0. 31875	1. 6011	5. 6210	7. 200
41	67	68	2031	27	11	
42	67	65	2186	42	12	
43	.66	63	2340	57	12	
44	66	61	2494	73	13	
45 46 47 48 49	65 64 63 63 62	59 57 55 53 51	2647 2800 2953 3104 3255	1. 6088 1. 6103 18 33 48	13 14 15 15	
50	8. 509 7161	8. 512 6448	o. 33406	. 1. 6163	5. 6216	
51	60	46	3556	77	17	
52	60	44	3706	1. 6192	18	
53	59	42	3 ⁸ 55	1. 6207	18	
54	58	40	4004	21	19	
55	57	38	4152	36	20	
56	57	35	4300	51	20	
57	56	33	. 4447	65	21	
58	55	31	4594	80	22	
59	55	29	4740	1. 6294	22	
60	8. 509 7154	8. 512 6427	0. 34885	1. 6308	5. 6223	7. 229

LATITUDE 5°.

Lat.	log A'	$ \frac{\log B}{\dim r'' = -0.04} $	log C	$ \frac{\log D}{\text{diff. } \mathbf{r''} = +0.22} $	log E	log F
5 00 I 2 3 4	8. 509 7154 53 53 52 51	8. 512 6427 24 22 20 18	ō. 34885 5030 5175 5320 5464		\$\bar{5}\$. 6223 24 24 25 26	7. 229
°5 6 7 8 9	50 49 49 48 47	15 13 11 08 06	5607 5750 5892 6034 6176	79 1. 6393 1. 6407 21 35	26 . 27 28 28 29	
10 11 12 13	8. 509 7146 46 45 44 43	8. 512 6404 6402 6399 97 95	o. 36317 6457 6597 6737 6876	1. 6449 63 77 1. 6491 1. 6504	5. 6230 30 31 32 32	
15 16 17 18	43 42 41 40 39	92 90 88 85 83	7015 7154 7292 7429 7566	18 32 45 59 72	33 34 34 35 36	
20 21 22 23 24	8. 509 7139 38 37 36 35	8. 512 6381 78 76 73 71	0. 37703 7839 7975 8111 8246	1. 6586 1. 6599 1. 6612 26 39	5. 6236 37 38 38 39	7. 256
25 26 27 28 29	35 34 33 32 31	69 66 64 61 59	8380 8514 8648 8781 8914		40 41 41 42 . 43	
30 31 32 33 34		8. 512 6356 54 52 49 47			5. 6243 44 45 46 46	
35 36. 37 38 39	27 26 25 24 23	44 42 39 37 34	9704 9834 0. 39964 0. 40094 0223	82 1. 6795 1. 6808 20 33	47 48 48 49 50	
40 41 42 43 44	8. 509 7122 21 21 20 19	8. 512 6332 29 27 24 21	o. 40351 0480 0608 0735 0863	1. 6846 58 · 71 83 1. 6896	5. 6251 51 52 53 54	7. 282
45 46 47 48 49	18 17 16 16	19 16 14 11	0990 1116 1242 1368 1493	1. 6908 21 33 45 58	54 55 56 57 57	
50 51 52 53 54	8. 509 7114 13 12 11	8. 512 6306 03 6301 6298 96	o. 41619 1743 1868 1992 2115	1. 6994	5. 6258 59 60 60 61	
55 56 57 58 59	09 09 08 07 06	93 90 88 85 82	2239 2362 2484 2607 2729	31 43 5.5 67 79	62 63 63 64 65	
60	8. 509 7105	8. 512 6280	0. 42850	1. 7090	5. 6266	7. 306

LATITUDE 6°.

Lat.	diff. r'' = -0.02	$ \frac{\log B}{\text{diff. } \mathbf{r''} = -0.05} $	log C	log D diff. 1"=+0.18	log E	log F
6 00 I 2 3 4	04 03 02 01	8. 512 6280 77 74 72 69	ō. 42850 2972 3093 3213 3334	1. 7090 1. 7102 14 26 38	5. 6266 67 67 68 69	7. 306
°5 6 7 8 9	7100 7099 98 97	66 64 61 58 55	3454 3573 3693 3812 3931	50 61 73 85 1. 7196	70 70 71 72 73	
10 11 12 13 14	8. 509 7096 95 94 93 92	8. 512 6253 50 47 44 42	4167 4285 4402 4519	1. 7208 19 31 42 54	5. 6274 74 75 76 77	
15 16 17 18	91 91 90 89 88	39 36 33 31 28	4636 4753 4869 4985 5101	65 76 88 1. 7299 1. 7310	78 78 79 80 81	
20 21 22 23 24	8. 509 7087 86 85 84 83	8. 512 6225 22 19 16 14	o. 45216 5331 5446 5560 5674	1. 73 ² 2 33 44 55 66	5. 6282 83 83 84 85	7. 329
25 26 27 28 29	82 81 80 79 78	11 08 05 6202 6199	5788 5902 6015 6128 6241	78 1. 7389 1. 7400 11 22	86 87 88 88 89	
30 31 32 33 34	8. 509 7077 76 75 74 73	8. 512 6196 94 91 88 85	o. 46353 - 6465 6577 6689 6800	1. 7433 44 54 65 76	5. 6290 91 92 93 93	
35 36 37 38 39	72 71 70 70 69	82 79 76 73 70	6911 7022 7132 7242 7352	87 1. 7498 1. 7508 19 30	94 95 96 97 98	
40 41 42 43 44	8. 509 7068 67 66 65 64	8. 512 6167 64 61 58 55	0. 47462 7571 7681 7789 7898	1. 7541 51 62 73 83	5. 6299 5. 6299 5. 6300 01 02	7.351
45 46 47 48 49	63 62 61 60 59	52 49 46 43 40	8006 8114 8222 8330 8437	1. 7594 1. 7604 15 25 36	03 04 05 06 06	
50 51 52 53 54	8. 509 7058 57 56 55 53	8. 512 6137 34 31 28 25	o. 48544 8651 8757 8864 8970	1. 7646 56 67 77 87	5. 6307 08 09 10	
55 56 57 58 59	52 51 50 49 48	22 19 16 13	9075 9181 9286 9391 9496	1. 7698 1. 7708 18 28 38	12 13 13 14 15	
60	8. 509 7047	8. 512 6107	0.49600	1. 7749	5. 6316	7.371

LATITUDE 7°.

Lat.	$ \begin{array}{c} \log A' \\ \text{diff. } \mathbf{i''} = -0.02 \end{array} $	log B diff. 1"=-0.06	log C	log D diff. 1"=+0.16	log E	log F
7 00 I 2 3	46 45 44	8. 512 6107 03 6100 6097	705 809 0. 49913	ī. 7749 59 69 79	\$\overline{5}\$. 6316 17 18	₹. 37 I
4 05 6 7 8	43 42 41 40 39 38	94 91 88 85 82 78	0. 50016 119 222 325 428 530	89 1. 7799 1. 7809 . 19 29 39	20 21 22 23 23 24	
10 11 12 13 14	8. 509 7037 36 35 34 33	8. 512 6075 72 69 66 62	o. 50632 734 836 o. 50937 o. 51039	1. 7849 59 68 78 88	5. 6325 26 27 28 29	
15 16 17 18	32 30 29 28 27	59 56 53 50 46	140 240 341 441 541	1. 7898 1. 7908 17 27 37	30 31 32 33 34	
20 21 22 23 24	8. 509 7026 25 24 23 22	8. 512 6043 40 37 33 30	o. 51641 741 840 o. 51939 o. 52038	1. 7946 56 66 75 85	5. 6335 36 37 37 38	7. 391
25 26 27 28 29	21 20 19 17 16	27 23 20 17 14	137 236 334 432 530	1. 7994 1. 8004 13 23 32	39 40 41 42 43	
30 31 32 33 34	8. 509 7015 14 13 12	8. 512 6010 07 04 6000 5997	o. 52628 725 822 o. 52919 o. 53016	1. 8042 51 61 70 79	5. 6344 45 46 47 48	
35 36 37 38 39	10 29 07 06 05	94 90 87 83 80	209 306 402 497	89 1. 8098 1. 8107 17 26	49 50 51 52 53	
40 41 42 43 44	8. 509 7004 03 02 01 7000	8. 512 5977 73 70 66 63	 53593 688 784 879 53973 	1. 8135 44 53 63 72	5. 6354 55 56 57 58	7. 409
45 46 47 48 49	6998 97 96 95 94	60 56 53 49 46	o. 54068 162 257 351 444	81 90 1. 8199 1. 8208 17	59 60 61 62 63	
50 51 52 53 54	8. 509 6993 91 90 89 88	8. 512 5942 39 35 32 28	o. 54538 631 725 818 o. 54911	1. 8226 35 44 53 62	5. 6364 65 66 67 68	
55 56 57 58 59	87 86 84 83 82	25 21 18 14 11	o. 55003 096 188 280 *	71 80 89 1. 8298 1. 8307	69 70 71 72 73	
60	8. 509 6981	8. 512 5907	0. 55464	1. 8315	5. 6374	7. 427

.

LATITUDE 8°.

1 80 04 555 24 75 2 70 5000 646 33 76 3 77 5897 738 42 77 4 76 93 829 50 78 05 75 90 0.55010 59 79 6 74 86 0.5010 68 80 7 73 82 100 77 81 8 71 79 101 85 82 9 70 75 281 1.8394 83 10 8.509 6969 8.512 5872 0.56371 1.8403 5.6384 11 66 68 460 12 85 12 67 64 550 20 86 11 67 64 550 20 86 11 67 68 47 57 728 37 88 11 68 59 696 51 61 639 28 87 11 61 62 50 966 54 91 11 61 62 50 966 54 91 11 62 50 966 54 91 11 8 50 43 0.57083 71 93 10 8.509 6957 8.512 5835 0.57260 1.8488 5.6395 7.4444 11 61 62 50 96 54 91 12 7 61 46 0.56095 62 92 18 59 43 0.57083 71 93 19 58 30 172 79 94 20 8.509 6957 8.512 5835 0.57260 1.8488 5.6395 7.4444 21 52 20 611 21 19 22 54 28 436 1.8505 96 23 44 52 20 611 21 19 24 54 28 436 1.8505 97 25 51 17 698 30 5.6400 96 27 48 00 872 46 02 28 47 06 0.57059 55 03 29 46 8.509 6945 8.512 5798 0.58045 03 04 20 8.509 6945 8.512 5798 0.58045 03 04 21 8	Lat.	log A' diff. r''=-0.02	log B diff. r''=-0.06	log C	log D diff. 1"=+0.14	log E diff. 1"=+0.02	log F
11	8 og I 2 3 4 05 6 7 8	80 79 77 76 75 74 73 71	94 5900 5 ⁸ 97 93 90 86 82 79	555 646 738 829 0. 55919 0. 56010 100 191	24 33 42 50 59 68 77 85	75 76 77 78 79 80 81	7. 427
20	11 12 13 14 15 16 17 18	68 67 65 64 63 62 61 59	8. 512 5872 68 64 61 57 54 50 46 43	460 550 639 728 817 906 0. 56995 0. 57083	12 20 28 37 45 54 62 71	85 86 87 88 90 91 92	
26	20 21 22 23 24	8. 509 6957 56 54 53 52	8. 512 5835 32 28 24 20	o. 57260 348 436 523 611	1. 8488 1. 8496 1. 8505 1. 21	5. 6395 96 97 98 99	7• 444
31 43 94 218 80 07 32 42 91 304 88 08 33 41 87 390 1.85966 09 34 39 83 476 1.8604 10 35 38 79 562 13 11 36 37 75 647 21 12 37 36 72 732 29 13 38 34 68 818 37 14 39 33 64 903 45 15 40 8.509 6932 8.512 5760 0.58987 1.8653 5.6416 7.461 41 31 56 0.59072 61 18 18 19 19 43 28 49 241 77 20 18 41 77 20 24 45 25 41 409 1.8603 22 22 46 24 37 493 1.8701 23 47 23 3	26 27 28	49 48 47	13 09 06	785 872 0. 57959	38 46 55	5. 6401 02 03	•
41 31 56 0. 59072 61 18 42 29 53 157 69 19 43 28 49 241 77 20 44 27 45 325 85 21 45 25 41 409 1. 8693 22 46 24 37 493 1. 8701 23 47 23 33 577 09 24 48 22 29 660 17 25 49 20 26 744 25 26 50 8. 509 6919 8. 512 5722 0. 59827 1. 8733 5. 6428 51 18 18 910 41 29 52 16 14 0. 59993 49 30 53 15 10 0. 60076 57 31 54 14 06 159 65 32 55 12 5702 241 73 33 56 11 <td< td=""><td>31 32 33 34 35 36 37 38</td><td>43 42 41 39 38 37 36 34</td><td>94 91 87 83 79 75 72 68</td><td>218 304 390 476 562 647 732 818</td><td>80 88 1.8596 1.8604 13 21 29</td><td>07 08 09 10 11 12 13 14</td><td></td></td<>	31 32 33 34 35 36 37 38	43 42 41 39 38 37 36 34	94 91 87 83 79 75 72 68	218 304 390 476 562 647 732 818	80 88 1.8596 1.8604 13 21 29	07 08 09 10 11 12 13 14	
50 8. 509 6919 8. 512 5722 0. 59827 1. 8733 5. 6428 51 18 18 910 41 29 52 16 14 0. 59993 49 30 53 15 10 0. 60076 57 31 54 14 06 159 65 32 55 12 5702 241 73 33 56 11 5698 324 81 34 57 10 94 406 89 35 58 09 90 488 1. 8796 37 59 07 86 570 1. 8804 38	41 42 43 44 45 46 47 48	31 29 28 27 25 24 23 22	56 53 49 45 41 37 33 29	o. 59072 157 241 325 409 493 577 660	61 69 77 85 1. 8693 1. 8701 09	18 19 20 21 22 23 24 25	7. 461
57 10 94 406 89 35 58 09 90 488 1.8796 37 59 07 86 570 1.8804 38	50 51 52 53 54	8. 509 6919 18 16 15 14	8. 512 5722 18 14 10 06 5702	o. 59827 910 o. 59993 o. 60076 159	1.8733 41 49 57 65	5. 6428 29 30 31 32 33	
00 0,500 0000 0,512 5002 0,00052 T XXT2 F 0.420 # 4#6	57 58	10 09 07	94 90	406 488	89 1. 8796	35	7. 476

LATITUDE 9°.

Lat.	$ \frac{\log A'}{\text{diff. } \mathbf{i''} = -0.02} $	log B diff. r''=-0.07	log C	log D diff. 1"=+0.12	log E diff. 1''=+0.02	log F
o , 9 00 I 2 3 4 05 6 7 8 9	8. 509 6906 05 03 02 6901 6899 98 97	8. 512 5682 78 74 70 66 62 58 54 50 46	ō. 60652 733 815 896 o. 60977 o. 61058 139 220 301 881	T. 8812 20 27 35 43 51 58 66 74 81	5. 6439 40 41 42 44 45 46 47 48 49	₹. 476
10 11 12 13 14 15 16 17 18	8. 509 6893 91 90 89 87 86 84 83 82 80	38 34 30 26 22 18 14	o. 61461 542 622 702 781 861 o. 61941 o. 62020 099 178	1. 8889 1. 8897 1. 8904 12 19 27 . 34 42 50	5. 6450 52 53 54 55 56 57 59 60 61	
20 21 22 23 24 25 26 27 28 29	8. 509 6879 78 76 75 74 72 71 69 68 67	5598 93 89 85 81 77 73 69	o. 62257 336 415. 493 572 650 728 806 884 o. 62962	1.8964 72 79 87 1.8994 1.9002 09 17 24 31	5. 6462 63 65 66 67 68 69 70 72 73	7. 490
30 31 32 33 34 35 36 37 38	64 62 61 60 58 57	52 48 43 39 35 31	117 194 271 349 426 502 579	1, 9039 46 53 61 68 75 82 90	5. 6474 75 76 78 79 80 81 83 84	
39 40 41 42 43 44 45 46 47 48	8. 509 6851 8. 509 6851 48 47 43 41 40	8. 512 5518 14 10 05 5501 4 5497 92 88 84	656 73 ² o. 638o8 885 o. 63961 o. 64037 112 188 264 339 415	1. 9097 1. 9104 1. 9111 19 26 33 40 47 54 61 69	85 5. 6486 87 89 90 91 92 94 95 96	7. 505
50 51 52 53 54 55 56 57 58 59	8. 509 6837 3.3 3.3 3.3 3.3 3.3 3.3 2.8 2.2 2.3	8. 512 5475 71 67 62 58 54 49 45 40	490 o. 64565 640 715 789 864 o. 64938 o. 65013 o87 161 235	1. 9197 1. 9204 11 18 25 32	97 5. 6498 5. 6500 01 02 03 05 06 07 08 10	
60		8. 512 5432		1. 9253	5. 6511	7.51

COAST AND GEODETIC SURVEY.

LATITUDE 10°.

Lat.	log A' diff. I''=-0.03	log B diff. r''=-0.08	log C	log D diff. r"=+o.rr	log E diff. 1''=+0.02	log F
0 00 I 2 3 4 05 6 7 8 9	8. 509 6822 21 19 18 17 15 14 12 11	8. 512 5432 27 23 19 14 10 05 5401 5396 92	ō. 65309 383 456 530 603 677 750 823 896 o. 65968	7. 9253 60 67 74 80 87 1. 9294 1. 9301 08	\$\overline{5}\$. 6511 12 13 15 16 17 18 20 21 22	7. 518
10 11 12 13 14 15 16 17 18	8. 509 6808 06 05 03 02 6800 6799 97 96 94	8. 512 5388 83 79 74 70 65 61 56 52 47	o. 66041 114 186 259 331 403 475 547 619 691	1. 9322 28 35 42 49 56 62 69 76 82	5. 6524 25 26 27 29 30 31 33 34 35	
20 21 22 23 24 25 26 27 28 29	8. 509 6793 91 90 88 87 85 84 82 81	8. 512 5343 38 33 29 24 20 15 11 06 5302	o. 66762 834 905 o. 66976 o. 67047 118 189 260 331 401	1. 9389 1. 9396 1. 9403 09 16 23 29 36 42 49	5. 6536 38 39 40 42 43 44 46 47 48	7. 532
30 31 32 33 34 35 36 37 38 39	8. 509 6777 76 74 73 71 70 68 67 65 64		0. 67472	1. 9456 62 69 75 82 88 1. 9495 1. 9501 08	5. 6549 51 52 53 55 56 57 59 60 61	
40 41 42 43 44 45 46 47 48 49	8. 509 6762 60 59 57 56 54 53 51 50 48	8. 512 5251 46 41 37 32 27 23 18 13 08	0. 68171 240 310 379 448 517 586 654 723 791	1. 9521 27 34 40 47 53 60 66 72 79	5. 6563 64 65 67 68 69 71 72 73 75	7. 544
50 51 52 53 54 55 56 57 58 59	8. 509 6746 45 43 42 40 38 37 35 34 32	8. 512 5204 5199 94 89 85 80 75 70 66 61	0. 68860 928 0. 68996 0. 69064 132 200 268 336 404 471	1. 9585 91 1. 9598 1. 9604 10 17 23 29 36 42	5. 6576 78 79 80 82 83 84 86 87 88	
60		8. 512 5156		1. 9648	5. 6590	7. 556

LATITUDE 11°.

Lat.	diff. i'' = -0.03	log B diff. 1"=-0.08	log C	log D diff. 1"=+0.10	$ \frac{\log E}{\dim I'' = +0.02} $	log F
° ' II 00 I 2 3 4 05 6 7 8	8. 509 6730 29 27 26 24 22 21 19 18 16	8. 512 5156 51 46 41 37 32 27 22 17	ō. 69539 606 673 740 807 874 0. 69941 0. 70008 974 141	7. 9648 54 61 67 73 79 86 92 1. 9698 1. 9704	. \$\overline{5}\$. 6590 91 93 94 95 97 98 5. 6599 5. 6601	₹. 556
10 11 12 13 14	8. 509 6714 13 11 09 08	5103 5098 93 88	0. 70208 274 340 406 473	1. 9710 16 23 29 35	5. 6604 05 06 08 09	
15 16 17 18	06 05 03 01 6700	8 ₃ 7 ⁸ 7 ₃ 68 6 ₃	539 604 670 736 802	41 47 53 59 65	11 12 13 15	
20 21 22 23 24	8. 509 6698 96 95 93 91	8. 512 5058 53 49 44 39	o. 70867 933 o. 70998 o. 71063 128	1. 9771 77 83 89 1. 9795	5. 6618 19 20 22 23	7. 568
25 26 27 28 29	90 88 86 85 83	34 29 24 19	194 259 323 388 453	1. 9801 07 13 19 25	25 26 27 29 30	
30 31 32 33 34	8. 509 6681 80 78 76 75	04 4999 94 89	0. 71518 582 647 711 775	1. 9831 37 43 49 55	5. 6632 33 35 36 37	
35 36 37 38 39	73 71 70 68 66	83 78 73 68 63	840 904 0. 71968 0. 72032 095	61 67 73 79 85	39 40 42 43 45	
40 41 42 43 44	8. 509 6665 63 61 59 58	8. 512 4958 53 48 43 38	0. 72159 223 286 350 413	1. 9890 1. 9896 1. 9902 08 14	5. 6646 47 49 50 52	7. 580
45 46 47 48 49	56 54 53 51 49	33 28 22 17 12	477 540 603 666 729	20 25 31 37 43	53 55 56 58 59	
50 51 52 53 54	8. 509 6647 46 44 43 41	8. 512 4907 4902 4897 92 86	0. 72792 855 918 0. 72980 0. 73043	1. 9949 54 60 66 72	5. 6661 62 64 65 66	
55 56 57 58 59	39 37 35 34 32	81 76 71 66 60	106 168 230 293 355	77 83 89 94 1.9900	68 69 71 72 74	
60	8. 509 6630	8. 512 4855	0. 73417	2. 0006	5. 6675	7. 591

LATITUDE 12°.

Lat.	$ \begin{array}{c c} \log A' \\ \text{diff. } \mathbf{1''} = -0.03 \end{array} $	$ \begin{array}{c} \log B \\ \dim x'' = -0.09 \end{array} $	log C	$ \frac{\log D}{\text{diff. } \mathbf{i''} = +0.09} $	$ \frac{\log E}{\text{diff. } \mathbf{r''} = +0.04} $	log F
0 /	0		derror		= //	=
12 00 I			ō. 73417 479	<u>2</u> . 0006	\(\bar{5}\). 6675	7. 591
2	29 27	50 45	4/9 54I	17	77 78	
3	25	39	603	23	80	
4	23	34	664	28	81	
05	21	29	726	34	83	
o 5 6	20	24	788	40	84	
7 8	18	18	849	45	86	
	16	13 0 8	911	51	87 89	
9	14	0 0	0. 73972	57	09	
10		8. 512 4803		2. 0062	5. 6690	
12	09	4797 92	094 156	6 ₇ 73	92 93	
13	07	87	217	79	95	
14	. 06	81	278	84	96	
15	04	76	339	90	98	
16.	02	7 I	399	2.0096	5. 6699	
17 18	6600 6599	65 60	460 521	2. 0101 07	5. 6701 02	
19	97	55	581	12	0.1	
20		8. 512 4749	0, 74642	2. 0118	5. 6705	7. 6oI
21	93	44	702	23	07	7.001
22	91	39	763	29	o 8	
23	90 88	33	823	34	10	
24	86	28	883	40	· II	
25 . 26	84	23 17	0. 749430. 75003	45 50	13 14	
27	82	12	063	56	16	
28	81	06	123	61	17	
29	79	4701	183	67	19	
30		8. 512 4696			5. 6720	
31 32	75	90 85	302 362	77 82		
33	73 72	79	422	8 ₃ 88	24 25	
34	70	74	481	94	27	
	68	68	540	2.0199	28	
35 36	66	63	600	2. 0205	30	
37 38	64	57	659	IO	3 1	
38 39	62 61	52 46	718 777	15 21	33	
					34	
40	8. 509 6559	8. 512 4641	0. 75836	2. 0226	5. 6736	7. 611
4I 42 '	57 55	35 30	895 0. 75954	32 37	37	
43	53	24	0. 75954	37 42	39 41	
44	51	19	072	47	42	
45	50	13	130	53	44	
46	48	08	189	53 58 6 ₃	45	
47 48	46	4602	247 206	63	47	
49	44 42	4597 91	3 0 6 364	69 74	48 50	
50		8. 512 4586				
51	8. 509 6540 39	80 80	0. 76422 481	2. 0279 84	5. 6751 53	
52	37		539	90	53 55 *	
53	35	75 69	597	2. 0295	56 58	
54	33	63	655	2. 0300		
55 56	31	58	713	05	59 61	
57	29 27	52 47	771 828	10 16	61 62	
57 58	25	41	886	21	64	
59	24	35	0. 76944	26	66	
60	8. 509 6522	8 512 4520	0. 77001	2. 0331	5. 6767	7. 621

LATITUDE 13°.

Lat.	$ \frac{\log A'}{\text{diff. } \mathbf{r''} = -\mathbf{o}.} $	log B .03 diff. 1"=-0.10	$ \frac{\log C}{\text{diff. } \mathbf{i''} = +0.93} $	$ \frac{\log D}{\text{diff. } \mathbf{r''} = +0.08} $	liff, 1"=+0.03	log F
o, , , , , , , , , , , , , , , , , , ,		22 8. 512 4536 20 2. 18 16 16 1; 14 0; 12 450; 10 4496 09 96 07 8,	4 059 116 3 174 7 231 2 288 6 346 9 403 5 460	2. 0331 36 42 47 52 57 62 67 73 78	\$\overline{3}\$. 6767 69 70 72 74 75 77 78 80 82	7. 62 I
10 11 12 13 14 15 16 17 18		03 8. 512 4473 01 69	3 0.77574 630 2 687 5 744 801 5 857 914 6.77970 7 0.78027	2. 0383 88 93 2. 0398 2. 0403 08 13 18 23 28	5. 6783 85 86 88 90 91 , 93 94 96 98	
20 21 22 23 24 25 26 27 28 29		8. 512 4410 82 10 80 4400 78 4399 76 93 74 87 70 76 68 70 66 6.	195 251 307 363 363 419 475 531 587	2. 0433 38 44 49 54 59 64 69 74 78	5. 6799 5. 6801 03 04 06 07 09 11 12 14	7. 631
30 31 32 33 34 35 36 37 38 39		54 8. 512 4358 53 52 59 41 57 35 55 29 53 23 51 17 49 11	7,54 809 865 920 0.78975 0.79030 0.86	2. 0483 88 93 2. 0498 2. 0503 08 13 18 23 28	5. 6816 17 19 20 22 24 25 27 29 30	
40 41 42 43 44 45 46 47 48 49	333332		0. 79251 306 360 415 470 525 579 634 688	2. 0533 38 42 47 52 57 62 67 72 76	5. 6832 34 35 37 39 40 42 44 45 47	7.640
50 51 52 53 54 55 56 57 58	2 I I	3 34 1 28 9 22 7 16 5 10 3 4204 1 4198 9 92	851 905 0. 79960 0. 80014 068 122 176 230	2. 0581 . 86 91 2. 0596 2. 0601 05 10 15 20 24	5. 6849 50 52 54 55 57 59 60 62 64	
60	8. 509 640	5 8. 512 4180	0. 80337	2. 0629	5. 6865	7. 649

10806°—11——3

COAST AND GEODETIC SURVEY.

LATITUDE 14°.

Lat.		odiff. 1"=−0.10	$ \log C $ diff. $\mathbf{r}'' = +0.87$	diff. r''=+0.0S	diff. i'' = +0.03	log F
° , 14 00 1 2 3 4	8. 509 6405 03 6401 6399 97	8. 512 4180 74 68 62 56	ō. 80337 391 445 498 552	2. o629 34 39 43 48	\(\bar{5}\). 6865 67 69 71 72	₹. 649
o5	95	50	605	53	74	
6	93	44	659	58	76	
7	91	38	712	62	77	
8	89	32	765	67	79	
9	87	26	819	72	81	
10	8. 509 6385	8. 512 4120	o. 80872	2. 0676	5. 6882	
11	83	14	925	81	84	
12	81	08	o. 80978	86	86	
13	79	4101	o. 81031	90	88	
14	77	4095	084	2. 0695	89	
15 16 17 18	75 73 71 · 69 67	89 83 77 71 65	137 190 243 295 348	2. 0700 04 09 14 18	91 93 94 96 98	v
20	8. 509 6365	8. 512 4059	o. 81401	2. 0723	5. 6900	7. 658
21	63	52	453	28	01	
22	61	46	506	32	03	
23	58	40	558	36	05	
24	56	34	611	41	06	
25	54	28	663	46	08	
26	52	21	715	51	10	
27	50	15	767	55	12	
28	48	09	820	60	13	
29	46	4003	872	64	15	
30 31 32 33 34	8. 509 6344 42 40 38 36	8. 512 3997 90 84 78 72	o. 81924 o. 81976 o. 82028 o80	2. 0769 73 78 83 87	5. 6917 19 20 22 24	
35	34	65	183	92	26	•
36	32	59	235	2. 0796	27	
37	29	53	287	2. 0801	29	
38	27	47	338	05	31	
39	25	40	390	10	33	
40	8. 509 6323	8. 512 3934	o. 82441	2. 0814	5. 6934	7. 667
41	21	28	493	19	36	
42	19	22	544	23	38	
43	17	15	596	28	40	
44	15	09	647	32	41	
45	13	3903	698	37	43	
46	11	3896	749	41	45	
47	08	90	800	46	47	
48	06	84	852	50	48	
49	04	77	903	54	50	
50	8. 509 6302	8. 512 3871	o. 82954	2. 0859	5. 6952	
51	6300	65	o. 83005	63	54	
52	6298	58	o55	68	55	
53	96	52	106	72	57	
54	94	45	157	77	59	
55 56 57 58 59	92 89 87 85 83	39 33 26 20	208 258 309 360 410	81 85 90 94 2. 0899	61 63 64 66 68	
60	8. 509 6281	8. 512 3807	0. 83461	2. 0903	5. 6970	7. 675

LATITUDE 15°.

Lat.	$ \begin{array}{c c} \log A' \\ \dim, 1'' = -0.04 \end{array} $	log B diff. 1''=-0.11	$\log C$ diff. $\mathbf{r}'' = +0.82$	log D diff. r''=+0.07	log E diff. 1"=+0.03	log F
0 / 15 00 I 2 3 4 05 6 7 8 9	8. 509 6281 79 77 74 72 70 68 66 64 62	8. 512 3807 3801 3794 88 81 75 68 62 56	ō. 83461 511 561 612 662 712 762 813 863 913	2. 0903 07 12 16 21 25 29 34 38 42	5. 6970 72 73 75 77 79 80 82 84 86	₹. 675
10 11 12 13 14 15 16 17 18	8. 509 6259 57 55 53 51 49 46 44 42 40	8. 512 3743 36 30 23 17 10 3704 3697 91 84	o. 83963 o. 84012 o62 112 162 212 261 311 361 410	2. 0947 51 55 59 64 68 72 77 81 85	5. 6988 89 91 93 95 97 5. 6999 5. 7000 02 04	
20 21 22 23 24 25 26 27 28 29	8. 509 6238 35 33 31 29 27 24 22 20 18		o. 84460 509 558 608 657 706 755 804 854	2. 0990 94 2. 0998 2. 1002 07 11 15 19 23 28	5. 7006 08 09 11 13 15 17 19 20 22	7. 683
30 31 32 33 34 35 36 37 38 39	8. 509 6216 14 11 09 07 05 02 6200 6198 96	8. 512 3612 3605 3598 92 85 79 72 65 59	o. 85001 049 098 147 196 245 293 342	2. 1032 36 40 44 49 53 57 61 65	5. 7024 26 28 30 31 33 35 37 39 41	
40 41 42 43 44 45 46 47 48 49	8. 509 6194 91 89 87 85 82 80 78 76	8. 512 3545 39 32 25 19 12 35°5 3498 92 85	0. 85439 487 536 584 633 681 729 777	2. 1074 78 82 86 90 94 2. 1099 2. 1103 07	5. 7042 44 46 48 50 52 54 55 57	7.691
50 51 52 53 54 55 56 57 58 59	8. 509 6171 69 67 64 62 60 58 55 53	8. 512 3478 71 65 58 51 44 38	o. 85922 o. 85970 o. 86018 o66 iii i6i 209 257 304	2. 1115 19 23 27 31 35 39 44 48 52	5. 7061 63 65 67 69 70 72 74 76 78	
60		8. 512 3411			5. 7080	7. 698

LATITUDE 16°.

Lat.	$ \frac{\log A'}{\text{diff. } \mathbf{i''} = -0.04} $	$ \begin{array}{c} \log B \\ \text{diff. } 1'' = -0.12 \end{array} $	$ \frac{\log C}{\text{diff. i''}=+0.77} $	log D diff. r''=+0.06	log E diff. 1''=+0.03	log F
, , , , , , , , , , , , , , , , , , ,	8. 509 6149 46 44 42 40	8. 512 3411 3404 3397 90 83	ō. 86400 447 495 542 590 637	2. 1156 60 64 68 72 76	\$\frac{1}{5}\$. 7080 \$2 84 85 87 89	7 . 698
o5 6 7 8 9	35 33 30 28	7° 63 56 49	684 73 ² 779 826	80 84 88 92	91 93 95 97	
10 11 12 13 14	8. 509 6126 24 21 19	8. 512 3342 35 28 22 15	o. 86873 921 o. 86968 o. 87015 062	2. 1196 2. 1200 04 08 12	5. 7099 5. 7101 03 04 06	
15 16 17 18	14 12 · 10 08 05	08 3301 3294 87 80	109 156 202 249 296	16 20 24 28 32	08 10 12 14 16	
20 21 22 23 24	8. 509 6103 6101 6098 96 94	8. 512 3273 66 59 52 45	o. 87343 389 436 483 529	2. 1236 40 44 47 51	5. 7118 20 22 24 25	7. 705
25 26 27 28 29	91 89 87 84 82	39 3 ² 25 18 11.	576 622 669 . 715 761	55 59 63 67 71	27 29 31 33 35	
30 31 32 33 34	8. 509 6080 77 75 73 70	3197 90 83 76	854 900 947 o. 87993	2. 1275 79 83 87 90	5. 7137 39 41 43 45	
35 36 37 38 39	68 66 63 61 59	69 62 55 48 41	o. 88039 085 131 177 223	94 2. 1298 2. 1302 06 10	47 49 51 52 54	
40 41 42 43 44	8. 509 6056 54 52 49 47	8. 512 3133 26 19 12 3105	o. 88269 315 360 406 452	2. 1314 17 21 25 29	5. 7156 58 60 · 62 64	7. 712
45 46 47 48 49	45 42 40 37 35	3098 91 84 77 70	498 543 589 634 680	33 37 40 44 48	66 68 70 72 -74	
50 51 52 53 54	8. 509 6033 30 28 26 23	8. 512 3063 56 48 41 34	o. 88726 771 816 862 907	2. 1352 56 59 63 67	5. 7176 78 80 82 84	
55 56 57 58 59	18 16 14 11	27 20 13 3006 2998	952 o. 88998 o. 89043 o88	71 74 78 82 86	86 88 90 92 94	
60	8. 509 6009	8. 512 2991	0. 89178	2. 1390	5. 7196	7. 719

LATITUDE 17°.

Lat.	$ \frac{\log A'}{\text{diff. } \mathbf{r''} = -0.04} $	log B diff. 1"=-0.12	$diff. \ i'' = +0.73$	log D diff. r"=+0.06	log E diff. r''=+0.03	log F
° ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' '	8. 509 6009 06 04 6002 5999 97 94 92 90	8. 512 2991 84 77 . 70 62 55 48 41 34	ō. 89178 223 268 313 358 403 448 493 538	2. 1390 93 2. 1397 2. 1401 04 08 12 16	5. 7196 97 99 5. 7201 03 05 07 09	7. 719
9 10 11 12 13 14	8. 500 5985 82 80 78 75	26 8. 512 2919 12 2905 2897 90 83	583 o. 89627 672 717 761 806	23 2. 1427 30 34 38 42 45	13 5. 7215 17 19 21 23 25	,
16 17 18	75 70 68 65 63	76 68 61 54	895 939 0. 89984 0. 90028	49 53 56 60	27 29 31 33	
20	8. 509 5961	8. 512 2846	0. 90072	2. 1464	5· 7 ² 35	7. 726
21	58	39	117	67	37	
22	56	32	161	71	39	
23	53	24	205	75	41	
24	51	17	249	78	43	
25	48	10	294	82	45	
26	46	2802	338	85	47	
27	44	2795	382	89	49	
28	41	88	426	93	51	
29	39	80	470	2. 1496	53	
30	8. 509 5936	8. 512 2773	0. 90514	2. I500	5· 7 ² 55	
31	34	66	558	04	57	
32	31	58	602	07	59	
33	29	51	646	II	61	
34	26	44	689	I4	64	
35 36 37 38 39	24 21 19 16	36 29 21 14 2707	733 777 821 864 908	18 22 25 29 32	66 68 70 72 74	
40	8. 509 5912	8. 512 2699	o. 90952	2. 1536	5. 7276	7.732
41	· 09	92	o. 90995	39	78	
42	07	84	o. 91039	43	80	
43	04	77	o82	47	82	
44	5902	69	126	50	84	
45	5899	62	169	54	86	
46	97	55	212	57	88	
47	94	47	256	61	90	
48	92	40	299	64	92	
49	89	32	342	68	94	
50	8. 509 5887	8. 512 2625	o. 91386	2. 1571	5. 7296	
51	84	17	429	75	5. 7298	
52	82	. 10	472	78	5. 7300	
53	79	2602	. 515	82	02	
54	77	2595	558	85	04	
55	74	87	601	89	06	
56	72	80	644	92	08	
57	69	72	687	96	11	
58	67	65	730	2. 1599	13	
59	64	57	773	2. 1603	15	
60	8. 509 5862	8. 512 2550	0. 91816	2. 1606	5. 7317	7. 738

LATITUDE 18°

Lat.	$\log A'$ $\operatorname{diff.} \mathbf{i''} = -0^{\circ}04$		$\frac{\log C}{\dim x'' = +0.70}$	log D	$ \log E $ $ \dim F = + \circ \circ_3 $	
° ,		5			_	= .
18 00	8.509 5862	8.512 2550	9.91816	2 ·1606	$\frac{1}{5}$.7317	· $\overline{7}$ ·738
I 2	59	42	859 9 02	10 13 ·	19 21	
3	57 54	35 27	945	13 -	23	
4	52	19	0.01082	20	25	
05	49	. 12	0.030	24	27	
05 6	46	8.512 2504	073	27	29	
7 8	44	8.512 2497	115	31	31	
9	41	89 81	158 201	34 38	33	
7	39		201	30	35	
IO	8.209 2836	8.512 2474	0.92243	2.1641	5.7337	
I I I 2	34 31	66	286 328	44 48	39 41	
13	29	59 51	371	51	44	
14	26	43	413	55	46	
15	24	36	456	58	48	
16	21	28	498	62	50	
17 18	19	20	540	6 5 68	52	
19	16	8.212 2405	582 625	72	54 56	
20 21	8.209 2811	8.512 2397	0.92667	2.1622	5.7358	7.744
22	o8 o6	90 82	709 751	79 82	60 62	
23	03	7.4	793	85	64	
24	8.209 2801	67	836	89	67	
25	8.509 5798	59	878	92	69	
26	96	51	920	95	71	
27 28 ·	93	44	0.92962	2.1699	73	
29	90 88	36 28	0°93004 046	2°1702 06	75 77	
30 31	8·509 5785 83 80 78	8.212 2320 13	0°93088 129	2·1709 12	5.7379 81	
32	80	8.212 2305	171	16	83	
31 32 33	78	8.212 2297	213	19	83 85 88	
34	75	90	255	22	88	
35 36 37 38	72	82	296	26	90	
30	70 67	74 66	338 380	29 32	9 2 94	
38	65	58	421 .	36 36	9 4 96	
39	65 62	51	463	39	5.4398	
40	8.509 5759	8.512 2243	0.93202	2.1745	5.7400	7.750
41	57	35	546 588	46	02	, , , ,
42	54	27	588	49	05	
43 44	52 49	19 12	629 671	52 56	0 7 09	
	46	8.512 2204				
45 46	44	8.212 2196	712 7 5 3	5 9 6 2	11	
47 48	41	88	795	65	15	
	39	80	836	69	17	
49	36	72	877	72	19	
50 51	8.509 5733	8.512 2165	0.93919	2.1772	5.7422	
51	31 28	57	0.93960	79 82	24	
52 53	28	49 41	0°94001 042	82 8e	26 28	
5 3 5 4	25 23	33	083	8 5 88	30	
	20	25	125	. 92	32	
56	18	17	166	95	34	
57	15	10	207	2.1498	37	
55 56 57 58 59	I 2 I 0	8·512 2102 8·512 2094	248 289	2°1801 05	39 41	
60	8.509 5707	8.512 2086	• 0°94330	2.1808	5.7443	7.756

LATITUDE 19°

Lat.	$\begin{array}{c c} \log A' \\ \text{diff. } \mathbf{r}'' = -0.04 \end{array}$	$\log B$ $\operatorname{diff.} \mathbf{1''} = -0.13$	$ \frac{\log C}{\dim T'' = +0.67} $	$\log D$ $\dim I'' = +0.02$	$\log E$ $\dim E' = +0.04$	
0 / 19 00 I 2 3 4	8·509 5707 04 8·509 5702 8·509 5699 96	8·512 2086 78 70 62 54	ō·94330 370 411 452 493	2·1808 11 14 18 21	₹·7443 45 47 49 52	₹.756
05 6 7 8 9	94 91 89 86 83	46 38 30 22 14	534 575 615 656 697	24 27 30 34 37	54 56 58 60 62	
10 11 12 13 14	8·509 5681 78 75 73 70	8.512 2006 8.512 1999 91 83 75	0·94737 778 819 859 900	2·1840 43 46 50 53 56	5·7464 67 69 71 73	
15 16 17 18 19	65 62 59 57	59 51 43 35	0·94981 0·95021 061 102	59 62 66 69	75 78 80 82 84	
20 21 22 23 24	8·509 5654 52 49 46 43	8·512 1927 19 11 8·512 1903 8·512 1895	0.95142 182 223 263 303	2·1872 75 78 81 84	5·7486 88 91 93 95	7 ·7 61
25 26 27 28 29	38 35 33 30	87 79 71 63 55	344 384 424 464 504	88 91 94 2·1897 2·1900	97 5·7499 5·7501 04 06	
30 31 32 33 34	8·509 5627 25 22 19 16	8·512 1847 38 30 22 14	0·95544 584 624 664 704	2°1903 07 10 13 16	5.7508 10 12 15	
35 36 37 38 39	14 11 08 06 03	8·512 1806 8·512 1798 90 82 74	744 784 824 863 903	19 22 25 28 31	19 21 23 26 28	ì
40 41 42 43 44	8·509 5600 8·509 5598 95 92 89	8·512 1766 57 49 41 33	0°95943 0°95983 0°96022 062 102	2°1934 38 41 44 47	5.7530 32 34 37 39	7.767
45 46 47 48 49	87 84 81 78 76	25 17 08 8·512 1700 8·512 1692	142 181 221 260 300	50 53 56 59 62	41 43 46 48 50	
50 51 52 53 54	8·509 5573 70 68 65 62	8°512 1684 75 67 59 51	0·96339 379 418 457 497	2°1965 68 71 74 77	5.7552 54 57 59 61	
55 56 57 58 59	59 57 54 51 48	43 34 26 18	536 575 615 654 693	80 83 86 89 92	63 65 68 70 72	
60	8.509 5546	8.512 1602	0.96733	2.1996	5°7574	7.772

LATITUDE 20°

Lat.	$\log A'$ $\operatorname{diff.} \mathbf{i''} = -0.05$	$\log B$ diff. $\mathbf{i''} = - \circ \mathbf{i}_4$	$\log C$ diff. i'' = +0.64	$\log D$ $\dim T'' = + 0.05$	$\log E$ $\dim x'' = + \circ \circ 4$	$\log F$ diff. $10' = +2.5$
o / 20 00 I 2 3 4	8·509 5546 43 40 37 35	8·512 1602 8·512 1593 85 77 68	ō·96733 772 811 850 889	2·1996 2·1999 2·2002 05 08	5·7574 77 79 81 83	7.772
05	32	60	928	11	86	
6	29	52	0°96967	14	88	
7	26	44	0°97006	17	90	
8	24	35	045	20	92	
9	21	27	084	23	94	
10 11 12 13	8.509 5518 15 12 10 07	8·512 1519 10 8·512 1502 8·512 1494 85	0·97123 162 201 240 279	2·2026 28 31 34 37	5.7597 5.7599 5.7601 03 06	
15 16 17 18	8·509 5501 8·509 5499 96 93	77 69 60 52 44	318 356 395 434 472	40 43 46 49 52	08 10 12 15 17	
20	8·509 5490	8·512 1435	0°97511	2°2055	5.7619	7.777
21	87	27	550	58	21	
22	85	18	588	61	24	
23	82	10	627	64	26	
24	79	8·512 1402	666	67	28	
25	76	8·512 1393	704	70	30	
26	73	85	743	73	33	
27	71	76	781	76	35	
28	68	68	819	79	37	
29	65	60	858	81	40	
30	8·509 5462	8·512 1351	0°97896	2·2084	5.7642	
31	59	43	935	87	44	
32	57	34	0°97973	90	46	
33	54	26	0°98011	93	49	
34	51	17	050	96	51	
35 36 37 38 39	48 45 42 40 37	8·512 1301 8·512 1292 84 75	088 126 164 203 241	2·2099 2·2102 05 08 10	53 55 58 60 62	
40	8·509 5434	8·512 1267	0°98279	2·2113	5·7664	7.782
41	31	58	317	16	67	
42	28	50	355	19	69	
43	25	41	393	22	71	
44	23	33	431	· 25	74	
45	20	24	469	28	76	
46	17	16	507	31	78	
47	14	8·512 1207	545	33	81	
48	11	8·512 1199	583	36	83	
49	08	90	621.	39	85	
50	8·509 5406	8·512 1182	0°98659	2.2142	5·7688	
51	03	73	697	45	90	
52	8·509 5400	64	735	48	92	
53	8·509 5397	56	773	50	94	
54	94	47	811	53	97	
55	91	39	848	56	5.7699	
56	88	30	886	59	5.7701	
57	86	21	924	62	04	
58	83	13	962	65	06	
59	80	8.512 1104	0°98999	67	08	
60	8.509 5377	8.212 1096	0.99034	2.5140	5.4411	7.787

LATITUDE 21°

Lat.	log A' diff. r'' = -0'05	log B diff. 1"=-0'15	$ \log C $ $ \dim x'' = +0.62 $	log D diff. 1" = +0.04	$ \log E $ diff. $\mathbf{i}'' = + \circ \circ_4$	$\log F$ $\operatorname{diff. 10'} = +2^{\circ}2$
° /	8·509 5377	8·512 1096	ō•99037	2·2170	5.7711	₹.787
21 00	74	87	075	73	13	
1 ·	71	79	112	76	15	
2 3	68	70	150	79	18	
4	66	62	187	81	20	
05	63	53	225	84	22	
6	60	45	262	87	24	
7	57	36	300	90	27	
8	54	27	337	93	29	
9	51	19	375	95	31	
10	8*509 5348	8*512 1010	0°99412	2°2198	5.7734	
11	46	8*512 1002	450	2°2201	36	
12	43	8*512 0993	487	04	38	
13	40	84	524	07	41	
14	37	76	562	09	43	
15 16 17 18	34 31 28 25 22	67 58 50 41 32	599 636 673 711 748	12 15 18 20 23	45 48 50 52 55	
20	8·509 5320	8·512 0924	0°99785	2·2226	5 *7757	7 .791
21	17	15	822	29	59	
22	· 14	8·512 0906	859	31	62	
23	11	8·512 0897	896	34	64	
24	08	89	933	37	66	
25	05	80	0'99971	40	69	
26	8*509 5302	71	1'00008 '	42	71	
27	8*509 5299	62	045	45	73	
28	96	54	082	48	76	
29	93	45	119	50	78	
30	8·509 5290	8·512 0836	1.00126	2°2253	5.7780	
31	88	27	192	56	83	
32	85	19	229	59	85	
33	82	10	266	61	87	
34	79	8·512 0801	303	64	90	
35	76	8·512 0792 .	340	67	92	
36	73	84	377	69	94	
37	70	75	413	72	97	
38	67	66	450	75	5*7799	
39	64	57	487	78	5*7802	
40 41 42 43 44	8·509 5261 58 55 52 49	8·512 0748 39 31 22 13	1.00524 560 597 634 670	2·2280 83 86 88 91	5·7804 06 09 11	7:796
45	46	8·512 0704	707	94 .	16	
46	44	8·512 0695	743	96	18	
47	41	86	780	2° 2299	20	
48	38	78	816	2° 2301	23	
49	35	69	853	04	25	
50 51 52 53 54	8·509 5232 29 26 23 20	8·512 0660 51 , 42 33 24	1.00890 926 962 1.00999 1.01032	2°2307 09 12 15	5·7828 30 32 35 37	
55	17	15	072	20	40	
56	14	8·512 0606	108	23	42	
57	11	8·512 0598	144	25	44	
58	08	89	181	· 28	47	
59	05	80	217	31	49	
60	8.509 5202	8.512 0571	1.01253	2.5333	5.4821	7.800

LATITUDE 22°

Lat.	$ \log A' \\ \text{diff. } \mathbf{i''} = -0.05 $	$ diff. \mathbf{r''} = -0.12 $	$ \frac{\log C}{\sin x'' = +0.29} $	$ \begin{array}{c} \log D \\ \text{diff. } \mathbf{i''} = + \circ \circ_4 \end{array} $	$ \log E $ diff. $\mathbf{r''} = + \circ \circ_4$	$ \log F $ $ \text{diff. 10'} = +2'6 $
0 /						
22 00	8.509 5202	8.512 0571	<u>1</u> .01253	2.2333	₹·7851	7.800
I	8.209 2199	62	289	36	54 56	•
3	96	53 44	326 362	38 41	56 50	
4	90	35	398	44	5 9 61	
05	87	26	434	46	63	
o <u>5</u> 6	84	17	470	49	63 66	
7 8	81	8.512 0508	506	51	68	
9	78 75	8·512 0499 90	542 578	54 57	71 73	
Io	8.509 5172	8.512 0481	1.01612		5.7875	
11	69	72	651	2·2359 62	78	
12	66	63	687	64	80	
13 14	63	54	7 23	67	83 85	
		45	759	70		
15 16	57 54	36 27	7 94 830	72 75	87 90	
17 18	51	18	866	7 7	92	
	48	09	902	80 82	95	
19	45	8.512 0400	938	83	97	
20 2 I	8.509 5142	8·512 0391 82	1.01974 1.02010	2·2385 88	5.7899	7.804
22	39 36	73	045	90	5·7 902 04	
23	33	64	081	93	07	
24	30	55	117	95	09	
25 26	27	46	153 188	2.2398	II	
27	24 21	37 28	224	2·2400 03	14 16	
28	18	19	260	06	19	
29	15	10	295	08	21	
30	8.509 5112	8·512 0301 8·512 0292 83	1 ·02331 367	2.5411	5.7924	
31 32	09 06	8.20292	367	13 16	26 28	
33	03	73	402 438	18	31	
34	8.509 5100	73 64	473	21	33	
35 36	8.509 5097	55 46	509	2 <u>3</u> 26	36 38	
30 37	94	40 37	544 580	20 28	38 41	
37 38	91 88	37 28	615	31	43	
39	85	19	651	33	45	
40	8.509 5082	8.512 0210	1.02686	2.2436	5.7948	7.808
4I	79 76	8.512 0200	721	38 41	50	
42 43	70 72	8.212 0191 82	757 792	41	53	
44	69	73	792 828	43 46	50 53 55 58	
45 46	66	64	863	48	60	
46	63 60	55	898	51	62	
47 48	57	55 46 36	933 1.02 969	48 51 53 56 58	65 67	
49	54	27	1.03004	58	70	
50	8.509 5051	8.512 0118	1.03039	2.5461	5.7972	
51	48 45	09	074	63	75	
52 53	45	8.512 0100 8.512 0000	109 145	63 66 68	77 80	
53 54	39	8·512 0090 81	180	70	82	
55	36	72 63	215	73	84	
55 56 57 58	33 30	63 54	250 285	75 78	8 7 89	
58	27	44	320	73 75 78 80	92	
59	23	. 35	355	83	94	
60	8.509 5020	8.512 0026	1.03390	2.2485	5.7997	7.812

LATITUDE 23°

Lat.	log A'	log B diff. 1" = -0.16	$\log C$ $\dim x'' = + \circ 57$	log D	$ \log E $ diff. $\mathbf{r}'' = + \circ \circ_4$	
0 /	8·509 5020	8·512 0026	T ·03390	2·2485	5.7997	₹·812
23 00	17	17	425	88	5.7999	
I	14	8·512 0008	460	90	5.8002	
2	11	8·511 9998	495	93	04	
3	08	89	530	95	07	
°5	05	80	565	2°2497	09	
6	8·509 5002	71	600	2°2500	12	
7	8·509 4999	61	634	02	14	
8	96	52	669	05	16	
9	93	43	704	07	19	
10	8·509 4990	8·511 9934	1°03739	2°2510	5.8021	
11	87	24	774	12	24	
12	83	15	809	14	26	
13	80	8·511 9906	843	17	29	
14	77	8·511 9896	878	19	31	
15 16 17 18	74 71 68 65 62	87 78 68 59 50	913 947 1°03982 1°04017 052	22 24 26 29 31	34 36 39 41 44	
20	8·509 4959	8·511 9840	1.04086	2 ² 534	5·8046	7 ·816
21	55	·31	121	36	49	
22	52	·22	155	38	51	
23	49	12	190	41	54	
24	46	8·511 9803	224	43	56	
25	43	8·511 9794	259	45	59	
26	40	84	293	48	61	
27	37	75	328	50	64	
28	34	66	362	53	66	
29	31	56	397	55	69	
30	8·509 4927	8·511 9747	1'04431	2 [·] 2557	5·8071	
31	24	37	466	60	74	
32	21	28	500	62	76	
33	18	19	534	64	79	
34	15	09	569	67	81	
35 36 37 38 39	09 05 8·509 4902 8·509 4899	8·511 97∞ 8·511 9690 81 71 62	603 637 672 706 740	69 71 · 74 76 78	84 86 89 91 93	
40	8·509 4896	8·511 9653	1.04775	2·2581	5°8096	7.819
41	93	43	809	83	5°8099	
42	90	34	843	85	5°8101	
43	87	24	877	88	04	
44	83	15	911	90	06	
45	80	8.511 9605	945	92	09	
46	77	8.511 9596	1°04980	95	11	
47	74	86	1°05014	97	14	
48	71	77	048	2°2599	16	
49	68	67	082	2 °2601	19	
50	8·509 4865	8·511 9558	1.05116	2°2604	5·8121	
51	61	48	150	06	24	
52	58	39	184	09	26	
53	55	29	218	11	29	
54	55	20	252	13	31	
55	49	10	286	16	34	
56	45	8·511 9501	320	18	36	
57	42	8·511 9491	3 5 4	20	39	
58	39	82	388	23	41	
59	36	72	422	25	44	
60	8.509 4833	8.511 9463	1.05456	2°2627	5.8146	7.823

LATITUDE 24°

Lat.	$\log A'$ diff. $r'' = -0.05$	log B diff. r"=-o*16	log C diff. r''=+0.56	log D diff. 1"=+0'04	log E diff. 1"=+0.04	log F diff. 10'=+1'6
0 / · · · · · · · · · · · · · · · · · ·	8·509 4833 30 26 23 20	8·511 9463 53 44 34 24	T*05456 490 523 557 591	2·2627 29 31 34 36	₹·8146 49 51 54 57	7 ·823
05 6 7 8 9	17 14 10 07 04	8·511 9405 8·511 9396 86 77	625 658 692 726 760	38 41 43 45 47	59 62 64 67 69	
10 11 12 13	8·509 4801 8·509 4798 94 91 88	8.511 9367 58 48 38 29	1°05794 827 861 894 928	2°2650 52 54 56 59	5·8172 7 4 77 79 82	
15 16 17 18	85 82 78 75 72	19 09 8·511 9300 8·511 9290 81	962 1°05995 1°06029 062 096	61 63 65 68 70	85 87 90 92 95	
20	8·509 4769	8.511 9271	1°06130	2·2672	5.8197	7·826
21	66	61	163	74	5.8200	
22	62	52	197	· 77	02	
23	59	42	230	79	05	
24	56	32	263	81	07	
25	53	23	297	83	10	
26	50	13	330	85	13	
27	46	8·511 9203	364	88	15	
28	43	8·511 9194	397	90	18	
29	40	84	431	92	20	
30 31 32 33 34	8·509 4737 33 30 27 24	8·511 9174 65 55 45 35	1.06464 497 530 564 597	2·2694 96 2·2699 2·2701	5·8223 25 28 31 33	
35	20	26	630	05	36	
36	17	16	664	07	38	
37	14	8·511 9106	697	10	41	
38	11	8·511 9096	730	12	43	
39	07	87	763	14	46	
40	8·509 4704	8·511 9077	1°06797	2·2716	5·8249	7.829
41	8·509 4701	67	830	18	51	
42	8·509 4698	58	863	20	54	
43	94	48	896	23	56	
44	91	38	929	25	59	
45	88	28	962	. 27	61	
46	85	18	1°06995	29	64	
47	81	8·511 9009	1°07028	31	67	
48	78	8·511 8999	061	33	69	
49	75	89	095	36	72	
50	8·509 4672	8·511 8979	1.07128	2·2738	5.8274	
51	68	70	161	40	77	
52	65	60	194	42	80	
53	62	50	226	44	. 82	
54	59	40	259	46	85	
55	55	30	292	49	87	
56	52	21	325	51	90	
57	49	11	358	53	92	
58	45	8·511 8901	391	55	95	
59	42	8·511 8891	424	57	5.8298	
60	8.509 4639	8.211 8881	1.07457	2.2759	5.8300	7.832

LATITUDE 25°

Lat.	log A diff. 1" = - 0.06	log B diff. 1" = -0'16	$\log C$ $\dim T'' = +0.54$	log D diff. r'' = + 0'03	$ \log \mathbf{E} $ diff. $\mathbf{r}'' = + \circ \circ_4$	$\log F$ $\dim \tau o' = + \tau \circ$
° / 25 00 I 2 3 4	8·509 4639 36 32 29 26	8·511 8881 71 62 52 42	T'07457 490 523 555 588	2·2759 61 63 66 68	5·8300 03 05 08 11	₹·832
05	23	32	621	70	13	
6	19	22	654	72	16	
7	16	12	687	74	18	
8	13	8·511 8802	719	76	21	
9	09	8·511 8793	752	78	24	
10 11 12 13	8·509 4606 03 8·509 4600 8·509 4596 93	8·511 8783 73 63 53 43	1.07785 817 850 883 915	2·2780 82 85 87 89	5·8 ₃₂ 6 29 32 34 37	
15 16 17 18	90 86 83 80 76	33 23 13 8·511 8704 8·511 8694	948 1°07981 1°08013 046 078	91 93 95 97 2°2799	39 42 45 47 50	
20	8·509 4573	8·511 8684	1.08111	2·2801	5.8352	7 ·835
21	70	74	143	03	55	
22	66	64	176	05	59	
23	63	54	208	07	60	
24	60	44	241	10	63	
25	56	34	273	- 12	66	
26	53	24	306	14	68	
27	50	14	338	16	71	
28	46	8·511 8604	370	18	73	
29	43	8·511 8594	403	20	76	
30	8·509 4540	8·511 8584	1.08435	2°2822	5 ^{.8} 379	
31	37	74	468	24	81	
32	33	64	500	26	84	
33	30	54	532	28	87	
34	26	44	565	30	89	
35	23	34	597	32	92	
36	20	24	629	34	94	
37	17	14	662	- 36	5.8397	
38	13	8·511 8504	694	38	5.8400	
39	10	8·511 8494	726	40	02	
40	8·509 4507	8·511 8484	1.08758	2·2842	5·8405	7.838
41	03	74	791	44	08	
42	8·509 4500	64	823	46	10	
43	8·509 4496	54	855	48	13	
44	93	44	887	50	16	
45	90	34	919	52	18	
46	86	24	951	54	21	
47	83	14	1°08984	56	24	
48	80	8·511 8404	1°09016	58	26	
49	76	8·511 8393	048	60	29	
50	8·509 4473	8·511 8383	1 '09080	2·2862	5.8431	
51	70	73	112	64	34	
52	66	63	144	66	37	
53	63	53	176	68	39	
54	60	43	208	70	42	
55	56	33	240	72	45	
56	53	23	272	74	47	
57	50	13	304	76	50	
58	46	8·511 8303	336	78	53	
59	43	8·511 8293	368	80	55	
60	8.509 4439	8.211 8283	1.09400	2.2882	5.8458	7.841

LATITUDE 26°

Lat.	$\log A'$ diff. $\mathbf{i''} = - \circ \circ \circ \circ \circ$	$\log B$ diff. $\mathbf{i''} = - \circ \mathbf{i}_7$	$ \frac{\log C}{\dim x'' = + \circ 52} $	$\log D$ $diff. 1'' = + \circ \circ_3$	$\log E$ diff. $\mathbf{r}'' = + \circ \circ_4$	$ \log F $ $ \dim F = + 1^{\circ}3 $
o / 26 00 I 2 3 4	8·509 4439 36 33 29 26	8·511 8283 72 62 52 42	T*09400 432 464 496 527	2·2882 84 86 88 90	5·8458 61 63 66 69	7 ·841
05	22	32	559	92	71	
6	19	22	591	94	74	
7	16	12	623	96	77	
8	12	8·511 8201	655	2°2898	79	
9	09	8·511 8191	687	2°2900	82	
10 11 12 13 14	8·509 4406 8·509 4402 8·509 4399 95 92	8·511 8181 71 61 51 40	1.09718 750 782 814 845	2·2902 04 06 08	5·8485 88 90 93 96	
15 16 17 18	88 85 82 78 75	30 20 10 8.211 8100 8.211 8089	877 909 940 1°09972 1°10004	12 14 16 18 20	5.8498 5.8501 04 06 09	
20	8·509 4372	8·511 8079	1·10036	2·2922	5·8512	7.844
21	68	69	067	23	14	
22	65	59	099	25	17	
23	61	48	130	27	20	
24	58	38	162	29	22	
25	54	28	194	31	25	
26	51	18	225	33	28	
27	48	8·511 8008	257	35	30	
28	44	8·511 7997	288	37	33	
29	41	87	320	39	36	
30	8·509 4337	8·511 7977	1°10351	2·294I	5·8539	
31	34	67	383	43	41	
32	31	56	414	45	44	
33	27	46	446	47	47	
34	24	36	477	48	49	
35	20	25	509	50	52	
36	17	15	540	52	55	
37	13	9.511 7905	571	54	57	
38	10	8.511 7895	603	56	60	
39	07	84	634	58	63	
40	8·509 4303	8·511 7874	1·10666	2·2960	5·8566	. 7.846
41	8·509 4300	64	697	62	68	
42	8·509 4296	53	728	63	71	
43	93	43	760	65	74	
44	89	33	791	67	76	
45	86	22	822	69	79	
46	83	12	854	71	82	
47	79	8·511 7802	885	73	85	
48	76	8·511 7791	916	75	87	
49	72	81	947	77	90	
50	8·509 4269	8·511 7771	1°10979	2°2978	5·8593	
51	65	60	1°11010	80	95	
52	62	50	041	82	5·8598	
53	58	40	072	84	5·8601	
54	55	29	103	86	94	
55 56 57 58 59	52 48 45 41 38	8·511 7709 8·511 7698 88 77	134 166 197 228 259	88 89 91 93 95	06 09 12 14 17	
60	8.509 4234	8.511 7667	1.11500	2*2997	5.8620	7.849

LATITUDE 27°

Lat.	$\log A'$ diff. $\mathbf{r}'' = -0.06$	$\log B$ diff. $\mathbf{r''} = -0.18$	$\log C$ diff. $r'' = +0.51$	$\log D$ diff. $\mathbf{r''} = +0.03$	$\log E$ diff. $\mathbf{r''} = +0.05$	log F diff. 10' = +1'1
o / 27 00 I 2 3 4	8·509 4234 31 27 24 20	8·511 7667 57 46 36 25	T·11290 321 352 383 414	2°2997 2°2909 2°3301 03 04	₹·8620 ?3 25 28 31	₹•849
05	17	15	445	06	34	
6	13	8·511 7605	476	08 -	36	
7	10	8·511 7594	507	10	39	
8	06	84	538	12	42	
9	03	73	569	14	44	
10 11 12 13	8·509 4200 8·509 4196 93 89 86	8·511 7563 53 42 32 21	1·11600 631 662 693 724	2·3015 17 19 21 23	5·8647 50 53 55 58	
15 16 17 18	82 79 75 72 68	8·511 7500 8·511 7490 79 69	755 786 817 848 878	24 26 28 30 32	61 64 66 69 72	
20	8·509 4165	8·511 7458	1°11909	2·3033	5 ⁸⁶ 75	7*851
21	61	48	940	35	77	
22	58	37	1°11971	37	80	
23	54	27	1°12002	39	83	
24	51	16	032	41	86	
25	47	8·511 7406	063	42	88	
26	44	8·511 7395	094	44	91	
27	40	85	125	46	94	
28	37	74	156	48	97	
29	33	64	186	50	5·8699	
30	8·509 4130	8·511 7353	1·12217	2°3051	5·8702	
31	26	43	248	53	05	
32	23	32	278	55	08	
33	19	22	309	57	10	
34	16	11	340	58	13	
35 36 37 38 39	8·509 4098	8·511 7301 8·511 7290 80 69 58	37° 401 432 462 493	60 62 64 65 67	16 19 22 24 27	
40	8·509 4094	8·511 7248	1·12523	2·3069	5·8 ₇₃ 0	7 ·853
41	91	37	554	70	33	
42	87	27	584	72	35	
43	84	16	615	74	38	
44	80	8·511 7206	646	76	41	
45	77	8·511 7195	676	78	44	
46	73	84	707	79	46	
47	70	74	737	81	49	
48	66	63	768	83	52	
49	63	53	798	85	55	
50	8*509 4059	8·511 7142	1·12829	2·3086	5 ^{.8} 757	
51	56	31	859	88	60	
52	52	21	889	90	63	
53	49	10	920	91	66	
54	45	8·511 7100	950	93	69	
55	41	8·511 7089	1°12981	95	72	
56	38	78	1°13011	97	74	
57	34	68	041	2·3099	77	
58	31	57	072	2·3100	80	
59	27	46	102	02	83	
60	8.509 4024	8.511 7036	1.13135	2.3104	5.8785	7.855

LATITUDE 28°

Lat.	$ \begin{array}{c} \log A' \\ \text{diff. } i'' = -0.06 \end{array} $	$ \log B $ $ \dim x'' = -0.18 $	log C diff. r" = +0.50	$ \begin{array}{c} \log D \\ \dim x'' = +0.03 \end{array} $	log E diff. 1" = +0.05	
0 /	-	-		_	= 0.0	=.0
28 00 I	8.509 4024	8·511 7036 25	<u>1</u> ·13132 163	2 ·3104 ⊃5	₹·8785 88	7·855
2	17	25 14	193	• • • • • • • • • • • • • • • • • • •	91	
3	13	8.211 7004	223	09	94	
4	10	8.511 6993	254	10	97	
05 6	06	82	284	12	5.8799	
7	8·509 4002 8·509 3999	72 61	314 345	14 16	5.8802	
7 8	95	50	375	17	05 08	
9	92	40	405	19	' 11	
10	8.509 3988	8.511 6929	1.13432	2. 3121	5.8813	
11	85 81	18	465	22	16	
12		8.511 6908	496	24	19	
13 14	78 74	8·511 6897 86	526 556	26 27	22 25	
	70		586	29	27	
15 16	67	75 65	616	31	30	
17 18	63	54	546	32	33 36	
18	60	43 33	677 707	34 36	36 39	•
20 2I	8.509 3952	8·511 6822 11	1·13737 767	2.3137	5.8841	7.857
22	49	8.211 2800	707 797	39 41	44 47	
23	42	8.511 6790	827	42	50	
24	38	79	857	44	53	
25 26	35	68	887	46	- 55	
	31 27	57 47	917 947	47 49	58 61	
27 28	24	36	1.13922	51	64	
29	20	25	1.14002	52	67	
30	8.509 3917	8.511 6714	1.14037	2.3124	5.8870	
31	13	8.511 6704	067	56	72	
32 33	09	8•511 6693 82	097 127	57 59 61	75 78 81	
33 34	8.509 3902	71	157	61	81	
35	8.509 3899	61	187	62	84	
36	95	50	217	64 65	8 7 89	
35 36 37 38	92 88	39 28	247 277	65 67	92	
39	84	17	307	69	95	
40	8.509 3881	8•511 6607	1.14337	2.3140	5.8898	7.859
41	77	8.211 6296	366	72	5.8901	, 3,
42	73	85	396 436	.74	04 06	
43 44	70 66	74 63	426 456	.74 75 77	09	
	63	52	486	78	12	
45 46	59	42	516	80	15 18	
47 48	55	31	545	82		
48 49	52 48	20 8 ·511 6 5 09	575 605	80 82 83 85	2 I 23	
50 51	8°509 3845 41	8 ·511 6498 87	1°14635 664	2°3187 88	5°8926 29	·
52	37	76 66	694	90	. 32	
53	34		724	91	35 38	
54	30	55	754 78a	93		
55 56	26 23	44 33	783 813	9 5 96	40 43	
57 58	19	22	843	98	46	
58		8:511 6400	872	2.3199	49 5 2	
59	12	8.511 6400	902	2.3201	52	
60	8*509 3808	8•511 6389	1.14935	2.3203	5.8955	7.861

LATITUDE 29°

Lat.	$ \log \mathbf{A}' \\ \text{diff. } \mathbf{r}'' = - \circ \circ 6 $	$ \begin{array}{l} \log B \\ \text{diff. } \mathbf{1''} = + 0.18 \end{array} $	$ \log C $ diff. $\mathbf{i''} = + 0.49$	$\log D$ diff. $\mathbf{r}'' = + \circ \circ_3$	$\log E$ diff. $\mathbf{r}'' = + \circ \circ \circ \circ \circ$	log F diff. 10' = + 0.8
o / 29 00 I 2 3 4	8·509 3808 05 8·509 3801 8·509 3797	8·511 6389 78 68 57 46	ī·14932 961 1·14991 1·15021 050	2·3203 c4 o6 o7 o9	₹•89 55 58 60 63 66	₹.861
o5 6 7 8	94 90 86 83 79 76	35 24 13 8.511 6302 8.511 6291	080 109 139 168 198	10 12 14 15	69 72 75 78 80	
10	8·509 3772	8.511 6280	1°15228	2·3218	5·8983	
11	68	69	257	20	86	
12	65	58	287	21	89	
13	61	47	316	23	92	
14	57	36	346	25	95	
15 16 17 18	54 50 46 43 39	26 15 8·511 6204 8·511 6193 82	375 405 434 464 493	26 28 29 31 32	5.8998 5.9000 03 06 09	
20	8·509 3735	8.511 6171	1·15522	2·3234	5.9012	7.863
21	32	60	552	35	15	
22	28	49	581	37	18	
23	24	38	611	38	21	
24	21	27	640	40	23	
25	17	16	670	42	26	
26	13	8·511 6105	699	43	29	
27	10	8·511 6094	728	45	32	
28	06	83	758	46	35	
29	8.509 3702	72	787	48	38	
30	8·509 3699	8.5116061	1·15816	2°3249	5 [.] 9 ⁰ 41	
31	95	50	846	51	43	
32	91	39	875	52	46	
33	88	28	904	54	49	
34	88	17	934	55	5 ²	
35	80	8·511 6006	963	57	55	
36	77	8·511 5995	1·15992	58	58	
37	73	84	1·16021	60	61	
38	69	73	051	61	64	
39	66	61	080	63	67	
40	8·509 3662	8.511 5950	1°16109	2·3264	5·9069	7.864
41	58	39	138	66	72	
42	55	28	167	67	75	
43	51	17	197	69	78	
44	47	8.511 5906	226	70	81	
45	44	8·511 5895	255	72	84	
46	40	84	284	73	87	
47	36	73	313	75	90	
48	33	62	343	76	93	
49	29	51	372	78	96	
50 51 52 53 54	8.509 3625 21 18 14	8·511 5840 29 18 8·511 5806 8·511 5795	1°16401 430 459 488 517	2·3279 81 82 84 85	5°9098 5°9101 04 07 10	
55 56 57 58 59	8.509 3603 8.509 3599 96 92	84 73 62 51 40	546 575 604 633 663	87 88 90 91 93	13 16 19 . 22 25	
60	8.209 3288	8.211 5729	1.16695	2*3294	5.9127	7.866

10806°—11——4

LATITUDE 30°

Lat.	$\log \mathbf{A}'$ diff. $\mathbf{r}'' = - \circ \circ \circ \circ \circ \circ$	log B diff. 1" = -0'19	$\log C$ diff. $\mathbf{r''} = + \circ \cdot 48$	$\log D$ diff. $r'' = + 0.02$	$\log E$ diff. $\mathbf{r''} = + \circ \circ \circ \circ$	$ \log F $ diff. $10' = +0$?
30 00	8·509 3588	8·511 5729	T·16692	2·3294	\$\overline{5}^{\cdot 9}\$127	₹.866
I	84	18	721	96	\$\overline{30}\$	
2	81	8·511 5706	750	97	33	
3	77	8·511 5695	778	2·3298	36	
4	73	84	807	2·3300	39	
o5	69	73	836	01	42	
6	66	62	865	03	45	
7	62	51	894	04	48	
8	58	40	923	06	51	
9	55	28	952	07	54	
10 11 12 13 14	8·509 3551 47 43 40 36	8·511 5617 8·511 5606 8·511 5595 84 · 73	1·16981 1·17010 039 068 097	2·3309 10 12 13 14	5.9157 59 62 65 68 71	
15 16 17 18 19	29 25 21 17	50 39 28 17	155 184 212 241	17 18 20 22	74 77 80 83	,
20 21 22 23 24	8·509 3514 10 06 8·509 3502 8·509 3499	8·511 5505 8·511 5494 83 72 61	1·17270 299 328 357 385	2°3323 24 26 27 29	5.9186 . 89 . 95 5.9198	7·867
25	95	49	414	30	5°9200	*
26	91	38	443	32	03	
27	88	27	472	33	06	
28	84	16	500	34	09	
29	80	8·511 5404	529	36	12	
30	8·509 3476	8·511 5393	1·17558	2·3337	5.9215	
31	72	82	587	39	18	
32	69	71	615	40	21	
33	65	59	644	41	24	
34	61	48	673	43	27	
35	57	37	701	44	30	
36	54	26	730	46	33	
37	50	14	759	47	36	
38	46	8·511 5303	788	48	39	
39	42	8·511 5292	816	50	42	
40	8·509 3439	8.511 5281	1·17845	2°3351	5*9245	7·86.9
41	35	69	874	53	48 ·	
42	31	58	902	54	51	
43	27	47	931	55	53	
44	24	35	959	57	56	
45	20	24	1·17988	58	59	
46	16	13	1·18017	59	62	
47	12	8·511 5202	045	61	65	
48	09	8·511 5190	074	62	68	
49	05	79	102	64	71	
50	8·509 3401	8·511 5168	1·18131	2°3365	5°9274	
51	8·509 3397	56	160	66	77	
52	94	45	188	68	80	
53	90	34	217	69	83	
54	86	22	245	70	86	
55 56 57 58 59	82 78 75 71 67	8·511 5100 8·511 5088 77 66	274 302 331 359 388	72 73 74 76 77	89 92 95 5'9298 5'9301	
60	8.209 3363	8.511 5054	1.18416	2.3379	5.9304	7.870

LATITUDE 31°

Lat.	$\log A'$ $\operatorname{diff.} r'' = -\circ \circ 6$	$ \log B $ diff. $\mathbf{I''} = -0.19$	$\log C$ $\dim C'' = +0.47$	$ \log D $ diff. $1'' = + 0^{\circ}02$	$\log E$ $\dim E + 0.05$	$\log F$ $\dim F \circ ' = + \circ ' \circ$
° ' ' 31 00 I 2 3 4	8·509 3363 60 56 52 48	8·511 5054 · 43 32 20 8·511 5009	T·18416 445 473 501 530	2·3379 80 81 · 83 84	\$\frac{1}{5}\cdot 9304 07 10 13 16	₹.870
05 6 7 8	44 41 37 33 29	8·511 4998 86 75 64 52	558 587 615 643 672	85 87 88 89 91	19 22 25 28 31	
10 11 12 13	8·509 3325 22 18 14 10	8·511 4941 29 18 8·511 4907 8·511 4895	1·18700 729 757 785 813	2·339 ² , 93 95 96 97	5 ·9334 3 7 39 42 45	
15 16 17 18	06 8.509 3303 8.509 3299 95 91	84 72 61 50 38	842 870 898 927 955	2°3399 2°3400 01 03 04	48 51 54 57 60	
20 21 22 23 24	8·509 3287 84 80 76 72	8·511 4827 15 8·511 4804 8·511 4793 81	1·18983 1·19012 040 068 096	2·3405 06 08 09 10	5·9363 66 69 72 75	7.871
25 26 27 28 29	68 65 61 57 53	70 58 47 35 24	125 153 181 209 238	12 13 14 16 17	78 81 84 87 90	
30 31 32 33 34	8·509 3249 46 42 38 34	8.511 4713 8.511 4701 8.511 4690 78 67	1·19266 294 322 351 379	2·3418 20 21 22 23	5.9393 96 5.9399 5.9402 05	
35 36 37 38 39	30 26 23 19	55 44 32 21 8·511 4609	407 435 463 491 520	25 26 27 29 30	08 11 14 17 20	
40 41 42 43 44	8·509 3211 07 03 8·509 3200 8·509 3196	8·511 4598 86 75 63 52	1·19548 576 604 . 632 660	2·3431 32 34 35 36	5·94 ² 3 26 29 3 ² 35	7*872
45 46 47 48 49	92 88 84 81 77	40 29 17 8·511 4506 8·511 4494	688 716 744 772 800	37 39 40 41 43	38 41 44 47 50	
50 51 52 53 54	8·509 3173 69 65 61 57	8·511 4483 71 60 48 37	1·19828 856 ° 884 912 940	2·3444 45 46 48 49	5·9453 56 59 62 65	
55 56 57 58 59	54 50 46 42 38	25 14 8·511 4402 8·511 4391 79	968 1°19996 1°20024 052 080	50 51 53 54 55	68 72 75 78 81	
60	8.509 3134	8.511 4368	1.50108	2.3456	5.9484	7.873

LATITUDE 32°

Lat.	$\log A'$ $\operatorname{diff.} \mathbf{i''} = -0.06$	log B diff. 1" = -0"19	$ \log C $ $ \dim x'' = + \circ \cdot 46 $	$\log D$	$ \log E $ $ \dim F = + \circ \circ \circ \circ $	$\log F$ $\dim F = + \circ \gamma$
0 / 32 00 I 2 3 4	8·509 3134 31 27 23 19	8·511 4368 56 44 33 21	T·20108 136 164 192 220	2·3456 57 59 60 61	₹.9484 87 90 93 96	7 ·873
05	15	8.511 4310	248	62	5.9499	
6	11	8.511 4298	276	64	5.9502	
7	07	87	304	65	05	
8	04	75	332	66	08	
9	8.509 3100	63	360	67	11	
10 11 12 13	8·509 3096 92 88 84 80	8·511 4252 40 29 17 8·511 4205	1·20387 415 443 471 499	2·3469 70 71 72 . 73	5.9514 17 20 23 26	
15 16 17 18	. 76 73 69 65 61	8·511 4194 82 71 59 47	527 555 582 610 638	75 76 77 78 79	29 32 35 38 41	
20	8·509 3057	8·511 4136	1 ·20666	2·3481	5 [.] 9544	7·874
21	53	24	694	82	47	
22	49	13	722	83	50	
23	46	8·511 4101	749	84	53	
24	42	8·511 4089	777	85	56	
25	38	78	805	87	60	
26	• 34	66	833	88	63	
27	30	54	860	89	66	
28	26	43	888	90	69	
29	22	31	916	91	72	
30	8·509 3018	8.511 4020	1·20944	2·3493	5 ·9575	
31	15	8.511 4008	971	94	78	
32	11	8.511 3996	1·20999	95	81	
33	07	85	1·21027	96	84	
34	8·509 3003	73	054	97	87	
35	8·509 2999	61	082	2'3499	° 90	
36	95	50	110	2'3500	93	
37	91	38	137	01	96	
38	87	26	165	02	5°9599	
39	83	15	193	03	5°9602	
40	8·509 2980	8·511 3903	1·21220	2·3504	5·9605	7 ·875
41	76	8·511 3891	248	06	08	
42	72	79	276	07	11	
43	68	68	303	08	15	
44	64	56	331	09	18	
45	60	44	358	10	21	
46	56	33	386	11	24	
47	52	21	414	13	27	
48	48	8·511 3809	441	14	30	
49	44	8·513 3798	469	15	33	
50	8·509 2940	8·511 3786	1·21496	2·3516	5·9636	
51	37	74	524	17	39	
52	33	63	551	18	42	
53	29	51	579	19	45	
54	25	39	607	21	48	
55	21	27	634	22	51	
56	17	16	662	23	54	
57	13	8·511 3704	689	24	58	
58	09	8·511 3692	717	25	61	
59	05	80	744	26	64	
60	8.509 2901	8.511 3669	1.21772	2.3527	5.9667	7.875

LATITUDE 33°

Lat.	log A' dıff. 1'' = -0'07	log B diff. 1'' =0°20	$\log C$ diff. $\mathbf{r}'' = +0.45$	$\log D$ $\dim T'' = +0.02$	log E diff. 1" = + 0.05	$ \log F $ $ \text{diff. 10'} = + 0' $
0 / 33 00 1 2 3 4	8·509 2901 8·509 2897 94 90 86	8·511 3669 . 57 . 45 . 33	T·21772 799 827 854 882	2·3527 29 30 31 32	₹°9667 70 73 76 79	₹.875
05	82	8.511 3610	909	33	82	
6	78	8.511 3598	937	34	85	
7	74	86	964	35	88	
8	70	75	1°21992	36	92	
9	66	63	1°22019	38	95	
10 11 12 13	8·509 2862 58 54 51 47	8·511 3551 39 28 16 8·511 3504	1·22047 074 101 129 156	2°3539 40 41 42 43	5°9698 5°9701 . 04 . 07 . 10	
15 16 17 18	43 39 35 31 27	8·511 3492 80 69 57 45	184 211 238 266 293	44 45 46 48 49	13 16 19 22 26	
20	8·509 2823	8.511 3433	1°22321	2°3550	5°9729	7.876
21	19	21	348	51	32	
22	15	8.511 3410	375	52	35	
23	11	8.511 3398	403	53	38	
24	07	86	430	54	41	
25	8*509 2803	74	457	55	44	
26	8*509 2799	62	485	56	47	
27	95	51	512	57	50	
28	91	39	539	58	53	
29	88	27	567	60	57	
30	8·509 2784	8.511 3315	1.22594	2·3561	5°9760	
31	80	8.511 3303	621	62	63	
32	76	8.511 3291	648	63	66	
33	72	80	676	64	69	
34	68	68	703	65	72	
35	64	56	73°	66	75	
36	60	44	757	67	78	
37	56	32	785	68	81	
38	52	20	812	69	85	
39	48	8.511 3209	839	70	88	
40	8.509 2744	8·511 3197	1°22866	2.3571	5.9791	7·876
41	40	85	893	72	94	
42	36	73	921	73	5.9797	
43	32	61	948	75	5.9800	
44	28	49	1°22975	76	03	
45	24	37	1°23002	77	06	
46	20	25	029	78	10	
47	16	13	057	79	13	
48	12	8.511 3102	084	80	16	
49	08	8.511 3090	111	81	19	
50 51 52 53 54	8·509 2704 8·509 2701 8·509 2697 93 89	8·511 3078 66 54 42 30	1 '23138 165 192 220	2·3582 83 84 85 86	5.9822 25 28 31 35	
55	85	18	274	87	38	
56	81	8·511 3006	301	88	41	
57	77	8·511 2995	328	89	44	
58	73	83	355	90	47	
59	69	71	382	91	50	
60	8.509 2665	8.511 2959	1.23409	2.3295	5.9853	7.877

LATITUDE 34°

Lat.	$\log A'$ $\operatorname{diff.} \mathbf{r''} = -\circ \circ_7$	log B diff. 1" = -0'20	$ \log C $ diff. $\mathbf{1''} = + \circ^{1}45$	$\log D$ diff. $\mathbf{1''} = +\mathbf{0'02}$	$ \log E $ diff. $\mathbf{r''} = +0.05$	$\log F$ $\operatorname{diff.} \operatorname{ro'} = + \circ \circ$
0 /	8·509 2665	· 8·511 2959	T·23409	2°3 5 92	₹·9 ⁸ 53	7 .877
34 00	61	47	437	93	57	
I	57	35	464	94	6c	
2	53	23	491	95	63	
3	49	8·511 2911	518	96	66	
05	45	8·511 2899	545	97	69	
6	41	87	572	98	72	
7	37	75	599	2°3599	75	
8	33	63	626	2°3600	79	
9	29	51	653	01	82	
10	8·509 2625	8·511 2840	1·23680	2·3602	5·9885	
11	21	28	707	03	88	
12	17	16	734	04	91	
13	13	8·511 2804	761	05	94	
14	09	8·511 2792	788	06	5·9897	
15 16 17 18	05 8·509 2601 8·509 2597 93 89	80 68 56 44 32	815 842 869 896 923	07 08 09 10 11	5·9901 04 07 10 13	
20	8·50¢ 2585	8·511 2720	1·23950	2·3612	5·9916	7·877
21	· 81	8·511 2708	1·23977	13	19	
22	77	8·511 2696	1·24004	14	23	
23	73	84	031	15	26	
24	69	72	058	16	29	
25 26 27 28 29	65 61 57 53 49	60 48 36 24	085 112 139 165 192	17 18 19 20 21	32 35 38 42 45	
30	8·509 2545	8·511 2600	1 ·24219	2·3622	5*9948	
31	41	8·511 2588	246	23	51	
32	37	76	273	24	54	
33	33	64	300	25	57	
34	29	52	327	26	61	
35 36 37 38 39	25 21 17 13	40 28 16 8·511 2504 8·511 2492	354 381 408 434 461	27 28 29 30 31	64 67 70 73 76	
40	8.509 2505	8·511 2480	1·24488	2·3632	5 [.] 9980	7 ^{.8} 77
41	8.509 2501	68	515	33	83	
42	8.509 2497	56	542	34	86	
43	93	44	569	35	89	
44	89	32	595	36	92	
45	85	20	622	37	96	
46	81	8·511 2408	649	38	5*9999	
47	77	8·511 2396	676	39	6*0002	
48	. 73	84	703	40	05	
49	69	72	729	41	08	
50	8·509 2465	8·511 2360	1.24756	2·3642	6·0011	
51	61	48	783	43	15	
52	57	35	810	43	18	
53	53	23	837	44	21	
54	49	8·511 2311	863	45	24	
55	45	8·511 2299	890	46	27	
56	41	87	917	47	31	
57	37	75	944	48	34	
58	33	63	970	49	37	
59	29	51	1°24997	50	40	
60	8.509 2425	8.511 2239	1 ·25024	2.3651	6.0043	7.877

LATITUDE 35°

Lat.	$ \frac{\log A'}{\text{diff. r'} = -0.07} $	$ \log B $ $ \dim x'' = -0.20 $	$ \begin{array}{c} \log C \\ \dim x'' = + \circ^{7} 44 \end{array} $	$ \begin{array}{c} \log D \\ \dim T = + o \cdot o I \end{array} $	$ \begin{array}{c} \log E \\ \text{diff. } \mathbf{r''} = + \text{ o'o5} \end{array} $	log F diff. 10' = +0'0
0 / 35 00 1 2 3 4	8·509 2425 21 17 13 09	8·511 2239 27 15 8·511 2203 8·511 2191	T·25024 050 077 104 131	2·3651 52 53 54 55		₹·877
05	05	78	157	56	59	
6	8·509 2401	66	184	56	63	
7	8·509 2396	54	211	57	66	
8	92	42	237	58	69	
9	88	30	264	59	72	
10	8·509 2384	8·511 2118	1·25291	2·3660	6*0075	
11	80	8·511 2106	317	61	79	
12	76	8·511 2094	344	62	82	
13	72	82	371	63	85	
14	68	70	397	64	88	
15 16 17 18	64 60 56 52 48	57 45 33 21 8·511 2009	424 451 477 504 531	65 66 66 67 68	91 95 6·0098 6·0101 04	
20	8·509 2344	8·511 1997	1·25557	2·3669	6.0107	7 ·877
21	40	85	584	70	11	
22	36	72	610	71	14	
23	32	60	637	72	17	
24	28	48	664	73	20	
25	24	36	690	74	23	
26	20	24	717	75	27	
27	16	12	743	75	30	
28	12	8·511 1900	770	76	33	
29	08	8·511 1887	796	77	36	
30	8·509 2304	8·511 1875	1·25823	2·3678	6*0140	•
31	8·509 2300	63	850	79	43	
32	8·509 2296	51	8 7 6	80	46	
33	92	39	903	81	49	
34	87	•27	929	82	52	
35 36 37 38 39	8 ₃ 79 75 71 67	8·511 1802 8·511 1790 78 66	956 1·25982 1·26009 035 062	82 83 84 85 86	56 59 62 65 69	
40	8·509 2263	8·511 1754	1·26088	2·3687	6.0172	7 ·877
41	59	41	115	88	75	
42	55	29	141	88	78	
43	51	17	168	89	81	
44	47	8·511 1705	194	90	85	
45	43	8·511 1693	221	91	88	
46	39	80	247	92	91	
47	35	68	274	93	94	
48	31	56	300	94	6·0198	
49	27	44	327	94	6·0201	
50	8·509 2222	8·511 1632	1·26353	2°369 5	6·0204	
51	18	20	380	96	07	
52	14	8·511 1607	406	97	11	
53	10	8·511 1595	432	98	14	
54	06	83	459	99	17	
55	8·509 2202	71	485	2·3699	20	
56	8·509 2198	58	512	2·3700	24	
57	94	46	538	01	27	
58	90	34	565	02	30	
59	86	22	591	03	33	
60	8.509 2182	8.511 1510	1.26617	2.3704	6.0237	7.877

LATITUDE 36°

Lat.	$\log A'$ $\operatorname{diff.} \mathbf{i''} = -\circ \circ_7$	log B diff. 1" = -0.50	log C	log D diff. r" = +o'or	log E diff. 1" = +0.05	$\log F$ $\operatorname{diff.} \ ro' = -o^{\bullet}$
° / 36 00 I 2 3 4	8·509 2182 78 74 70 65	8·511 1510 8·511 1497 85 73 61	7·26617 644 670 697 723	2·3704 04 05 06 07		₹.877
05 6 7 8 9	61 57 53 49 45	48 36 24 8·511 1412 8·511 1399	749 776 802 828 855	08 09 09 10	53 56 59 63 66	
10 11 12 13	8·509 2141 37 33 29 25	8·511 1387 75 63 50 38	1 · 26881 908 934 960 1 · 26987	2·3712 13 13 14 15	6·0269 - 72 76 79 82	
15 16 17 18	21 16 12 08 04	26 14 8·511 1301 8·511 1289 77	1·27013 039 066 092 118	16 17 17 18 19	85 89 92 95 6·0299	
20	8·509 2100	8·511 1265	1 ·27145	2·3720	6·0302	7.877
21	8·509 2096	52	171	2I	05	
22	92	40	197	2I	08	
23	88	28	223	22	12	
24	84	15	250	23	15	
25	80	8·511 1203	276	24	18	
26	75	8·511 1191	302	25	21	
27	71	79	329	25	25	
28	67	66	355	26	28	
29	63	54	381	27	31	
30	8·509 2059	8·511 1142	1·27407	2·3728	6·0334	
31	55	29	434	29	38	
32	51	17	460	29	41	
33	47	8·511 1105	486	30	44	
34	43	8·511 1092	512	31	48	
35	39	80	539	32	51	
36	35	68	565	32	54	
37	30	56	591	33	57	
38	26	43	617	34	61	
39	22	31	644	35	64	
40	8·509 2018	8.511 1019	1 · 27670	2·3735	6·0367	7.877
41	14	8.511 1006	696	36	7 I	
42	10	8.511 0994	722	37	74	
43	06	82	748	38	77	
44	8·509 2002	69	775	39	80	
45	8·509 1998	57	801	39	84	
46	93	45	827	40	87	
47	89	32	853	41	90	
48	85	20	879	42	94	
49	81	8·511 0908	905	42	6·0397	
50 51 52 53 54	8·509 1977 73 69 65 61	8·511 0895 83 71 58 46	1·27932 958 1·27984 1·28010 036	2·3743 44 45 45 46	6·0400 03 07 10	
55	56	34	062	47	17	
56	52	21	088	48	20	
57	48	8·511 0809	114	48	23	
58	44	8·511 0797	141	49	27	
59	40	84	167	50	30	
60	8.509 1936	8.511 0772	1.28193	2.3750	6.0433	7.876

LATITUDE 37°

Lat.	$ \begin{array}{c} \log A' \\ \dim, i'' = - \circ \circ_7 \end{array} $	log B diff. 1" = -0'21	$ \frac{\log C}{\text{diff. } \mathbf{i''} = + 0.43} $	log D diff. 1" = +0'01	$\log E$ $\dim E$	$ \log F $ $ \dim F = -0.3 $
o / 37 00 I 2 3	8·509 1936 32 28 23	8·511 0772 60 47 35	1·28193 219 245 271	2·3750 51 52 53		₹.876
4	19	22	297	53	46	
o5 6 7 8 9	15 11 07 8·509 1903 8·509 1899	8·511 0710 8·511 0698 85 73 61	324 350 376 402 428	54 55 56 56 57	50 53 56 60 63	
10 11 12 13 14	8·509 1895 90 86 82 78	8·511 0648 36 23 8·511 0611 8·511 0599	1 ·28454 480 506 532 558	2·3758 59 59 60 61	6.0466 70 73 76 80	
15 16 17 18	74 70 66 62 57	86 74 61 49 37	584 610 636 662 688	61 62 63 63 64	83 86 89 93 96	
20 21 22 23 24	8.509 1853 49 45 41 37	8.511 0524 12 8.511 0500 8.511 0487 75	1·28715 741 767 793 819	2·3765 66 66 67 68	6·0499 6·0503 06 09	7·876
25 26 27 28 29	33 28 24 20 . 16	62 50 37 25	845 871 897 923 949	68 69 70 70 71	16 19 23 26 29	
30 31 32 33 34	8·509 1812 08 04 8·509 1800 8·509 1795	8.511 0400 8.511 0388 75 63 51	1.28975 1.29001 027 053 079	2°3772 72 73 74 74	6·0533 36 39 43 46	
35 36 37 38 39	91 87 83 79 75	38 26 13 8·511 0301 8·511 0288	104 130 156 182 208	75 76 76 77 78	49 53 56 59 63	
40 41 42 43 44	8·509 1771 66 62 58 54	8·511 0276 64 51 39 26	1·29234 260 286 312 338	2·3779 79 80 81 81	6·0566 69 73 76 79	7.875
45 46 47 48 49	50 46 41 37 33	14 8·511 0201 8·511 0189 76 64	364 390 416 442 468	82 82 83 84 84	83 86 89 93 6•0596	
50 51 52 53 54	8.509 1729 25 21 16 12	8·511 0151 39 26 14 8·511 0102	1°29494 520 546 571 597	2·3785 86 86 87 88	6·0600 03 06 10	
55 56 57 58 59	08 04 8·509 1700 8·509 1696 92	8·511 0089 77 64 52 39	623 649 675 701 727	88 89 90 90 91	16 20 23 26 30	
60	8.509 1687	8.511 0027	1.29753	2.3792	6.0633	7.874

LATITUDE 38°

Lat.	log A' diff. 1" = -0.07	$ \begin{array}{c} \log B \\ \dim \mathbf{r}'' = - \circ \cdot \mathbf{2r} \end{array} $	$\log C$ $\dim x'' = + \circ^{\circ} 43$	log D diff. 1" = + 0*01	$ \log E $ $ \dim E $	$\log F$ $\dim F = - \circ$
0 / 38 00 I 2 3 4	8·509 1687 83 79 75 71	8·511 0027 14 8·511 0002 8·510 9989 77	T·29753 778 804 830 856	2·3792 92 93 93 94	₹ 0633 36 40 43 47	₹.874
o5	67	64	882	95	50	
6	62	52	908	95	53	
7	58	39	934	96	57	
8	54	27	959	97	60	
9	50	14	1*29985	97	63	
10 11 12 13 14	8·509 1646 42 37 33 29	8·510 9902 8·510 9889 77 64 52	1·30011 037 063 089 114	2·3798 2·3799 2·3800 00	6·0667 70 73 77 80	
15 16 17 18	25 21 17 12 08	39 27 14 8·510 9802 8·510 9789	140 166 192 218 243	01 02 02 03 03	84 87 90 94 6·0697	
20	8.509 1604	8·510 9777	1·30269	2·3804	6·0701	7 ·874
21	8.509 1600	64	295	05	04	
22	8.509 1596	52	321	05	07	
23	92	39	347	06	11	
24	87	27	372	06	14	
25 26 27 28 29	83 79 75 71 66	8.510 9701 8.510 9689 77 64	398 424 450 476 501	07 08 08 09 09	17 21 24 28 31	
30	8·509 1562	8·510 9652	1·30527	2·3810	6·0734	
31	58	39	* 553	11	38	
32	54	27	579	11	41	
33	50	14	604	12	44	
34	46	8·510 9601	630	12	48	
35	41	8·510 9589	656	13	51	
36	37	76	682	14	55	
37	33	64	707	14	58	
38	29	51	733	15	61	
39	25	39	759	15	65	
40	8.509 1521	8·510 9526	1°30785	2·3816	6·0768	7.873
41	16	14	810	16	72	
42	12	8·510 9501	836	17	75	
43	08	8·510 9488	862	18	78	
44	04	76	887	18	82	
45 46 47 48 49	8·509 1500 8·509 1495 91 87 83	63 51 38 26 13	939 965 1°30990 1°31016	19 19 20 20 21	85 89 92 95 6·0799	
50	8·509 1479	8·510 9401	1·31042	2·3822	6.0802	
51	75	8·510 9388	067	22	06	
52	70	76	093	23	09	
53	66	63	119	23	13	
54	62	50	144	24	16	
55	58	38	170	24	19	
56	53	25	196	25	23	
57	49	13	221	25	26	
58	45	8·510 9300	247	26	30	
59	41	8·510 9287	273	27	33	
60	8.509 1437	8.510 9275	1.31299	2.3827	6.0836	7.872

LATITUDE 39°

Lat.	$\log A'$ $\text{diff. } \mathbf{r''} = -0.07$	log B diff. 1"= - 0'21	. log C diff. r"=+o'43	$ \log D $ diff. $\mathbf{r}'' = + \mathbf{o} \cdot \mathbf{o} \mathbf{r}$	log E diff. r"= +0.06	$ \log F $ $ \dim F = -o' $
o / 39 00 I 2 3 4	8·509 1437 33 28 24 20	8·510 9275 62 50 37 25	T·31299 324 350 375 401	2·3827 28 28 29 29	ē∙o836 40 43 47 50	7 .8 72
o5 6 7 8	16 12 07 8·509 1403 8·509 1399	8.510 9212 . 8.510 9199 87 74 62	427 452 478 504 529	30 30 31 31 32	53 57 60 64 • 67	
10 11 12 13	8·509 1395 91 86 82 78	8·510 9149 36 24 8·510 9111 8·510 9098	1.31555 581 606 632 658	2·3832 33 33 34 35	6·0871 74 77 81 84	
15	74	86	683	35	88	
16	70	73	709	36	91	
17	65	61	734	36	9 5	
18	61	48	760	37	6•0898	
19	57	36	786	37	6•0902	
20	8°509 1353	8.510 9023	1'31811	2·3838	6.0905	7.871
21	49	8.510 9010	837	38	08	
22	44	8.510 8998	862	39	12	
23	40	85	888	39	15	
24	36	73	913	40	19	
25	32	60	939	40	22	
26	28	47	965	41	26	
27	23	35	1°31990	41	29	
28	19	22	1°32016	42	32	
29	15	8·510 8909	041	42	36	
30	8·509 1311	8·510 8897	1°32067	2·3843	6·0939	
31	07	84	092	43	43	
32	8·509 1302	72	118	44	46	
33	8·509 1298	59	144	44	50	
34	94	46	169	45	53	
35	90	34	195	45	57	
36	86	21	220	46	60	
37	81	8·510 8808	246	46	63	
38	77	8·510 8796	271	47	67	
39	73	83	297	47	70	
40	. 8·509 1269	8·510 8771	1°32323	2·3848	6°0974	7·870
41	64	58	348	48	77	
42	60	45	374	49	81	
43	56	33	399	49	84	
44	52	20	425	50	88	
45	48	8·510 8707	, 450	50	91	
46	43	8·510 8695	476	51	95	
47	39	82	501	51	6°0998	
48	35	69	527	52	6°1002	
49	31	57	552	52	05	
50	8·509 1227	8·510 8644	1.32578	2°3852	6·1008	
51	22	31	603	53	12	
52	18	19	629	53	15	
53	14	8·510 8606	654	54	19	
54	10	8·510 8593	680	54	22	
55	06	81	705	55	26	
56	8·509 1201	68	731	55	29	
57	8·509 1197	55	756	56	33	
58	93	43	782	56	36	
59	89	30	807	57	40	
60	8.209 1184	8.510 8517	1.32833	2.3857	6.1043	7.869

LATITUDE 40°

Lat.	log A' diff. 1"= -0.07	$ \log B $ $ \dim B = -0.21 $	$\log C$ $\dim T'' = +0.42$	log D diff. 1"=+o'01	log E diff. 1"=+0.06	log F diff. 10'=-0'
o / 40 00	8.200 1184	8.510 8517	ī·32833	2 .3857	_ 6.1043	₹.869
1 2 3	80 76 72 67	8·510 8505 8·510 8492 79 67	858 884 909	58 58 58	47 50 54 57	
4 05 6	63 59	54 41	93 5 960 1°32986	59 59 60	61 64	
7 8 9	55 50 46	29 16 8·510 8403	1·33011 037 062	60 61	67 71 74	
10	8.509 1142	8·510 8391 78	1.33088	2·3861 62	6·1078	
12 13 14	34 29 25	65 53 40	139 164 189	62 63 63	8 5 88 92	
15 16	21 17 12	27 15 8·510 8302	21 5 240 266	64 64 65	6·1102 6·1099 95	
17 18 19	08	8·510 8289 77	291 317	65 65	o6 o9	
20 21	8.209 1006 8.209 1100	8·510 8264 51	1.33345	2°3866 66	6.1113	7.867
22 23 24	91 87 83	38 26 13	393 418 414	67 67 68	20 23 27	
25 26 27	79 74 70	8·510 8200 8·510 8188 75	469 495 520	68 68 69	30 34 37	
27 28 29	66 62	62 50	546 571	69 70	4 I 44	
30 31 32 33 34	8·509 1057 53 49 45 41	8·510 8137 24 8·510 8111 8·510 8099 86	1°33596 622 647 673 698	2·3870 70 71 71 72	6°1148 51 55 58 62	
35 36 37 38 39	36 32 28 24 19	73 61 48 35 23	723 749 774 800 825	72 72 73 73 74	65 69 72 76 79	
40 41 42 43	8·509 1015 11 07 8·509 1002	8·510 8010 8·510 7997 . 84 72	1·33850 876 901 926	2·3874 74 75 75	6·1183 86 90 93	7·866
44 45 46 47 48	8·509 0998 94 90 85 81 77	59 46 33 21 8·510 7908 8·510 7895	952 1°33977 1°34003 028 053 079	76 76 76 77 77	6·1197 6·1200 04 07 11 15	
49 50 51 52 53	8·509 0973 68 64 60	8·510 7883 70 57 44	1°34104 129 155 180	2·3878 78 79 79	6·1218 22 25 29	
54 55 56	56	32 19	206 231	79 80	3 ² 36	
56 57 58 59	47 43 39 34	8·510 7806 8·510 7793 81 68	256 282 307 332	80 80 81 81	39 43 46 50	
60	8.509 0930	8.510 7755	1.34328	2.3882	6.1223	7.864

LATITUDE 41°

o / 4I OO 1 2 3 4 O5 6 7	8·509 0930 26 22 · 18 13	8·510 7755 42 30 17	ī·₃₄₃₅8 38ვ	<u>z</u> ·3882	₹.1253	= 0.0
41 00 1 2 3 4 05 6	26 22 18 13	42 30 17	383		<u></u>	=.04
2 3 4 05 6	26 22 18 13	42 30 17	383		0 4 2 1 1	7 .864
3 4 05 6	· 18 13	17		82	57 60	• •
4 05 6	13		408	82		
o ₅	09	8.210 7704	434 459	83 83	64 67	
6 7						
7	05	8.210 2691	484 510	83 84	71	
	8.200 0000	79 66	535	84	75 78 82	
7 8	8.509 0896	53	560	84	82	
9	92	40	586	85	85	
10	8.509 0888	8.510 7628	1.34611	2.3885	6.1589	
II	83	15	636		92	
12	7 9	8.210 2605	662	8 ₅ 86	96	
13	75	8.510 7590	687	86	6.1299	
14	71	77	712	87	6.1303	
15	67 62	64	738	87	06	
	58	5 I 39	763 788	8 7 88	10 14	
17	54	26	814	88	17	
19	49	13	839	88	21	
20	8.509 0845	8.510 7500	1.34864	2.3889	6.1324	7.863
21	41	8.510 7488	. 890	89	28	7 003
22	37	75 62	915	89	31	
23	32 28		940	90	35 38	
24		49	965	90		
25	24	36	1.34991	90	42	
26	20 15	24 8.510 7411	1°35016 041	91 91	46 49	
27 28	11	8.510 7398	066	91	53	
29	07	85	092	91	53 56	
30	8.509 0803	8.510 7373	1.35117	2.3892	6.1360	
31	8.509 0798	60	142	92		
32	94	47	168	92	63 67	
32 33 34	90 86	34 22	193 218	93	70 7 4	•
				93		
35 36	81 77	8·510 7309 8·510 7296	243 269	93 94	78 81	
37	73	83	294	94	85	
37 38	69	70 58	319	94	85 88	
39'	64	58	345	95	92	
40	8.509 0760	8.510 7245	1.35370	2.3895	6.1395	7.861
4 I	56	32	395 420	95	6.1399	, 551
42	52	19	420	95 96	6.1403	
43	47 43	8·510 7207 8·510 7194	446 471	96 96	06 10	
45 46	39 35	81 68	496 522	97 97	13 17	
47	35 30 26	55	547	97 97	20	
47 48	26	43	572	97 98	24 28	
49	22	30	597	98	28	
50 51	8.509 0718	8.510 7117	1.35623	2.3898	6.1431	
51	13	8.210 2104	648	98 98		
5 ² 53	09	8.210 2091	673 698	98	38	
54	o5 8·509 0700	79 66	698 723	99 99	35 38 42 46	
1						
55 56	8.209 0696	53 40	749 7 74	2°3899 2°3900	49	
57	92 88	27	774 799	2 3900	53 56 60	
57 58 59	83	15	824	00	60	
59	79	8.510 7002	850	00	63	
60	8.509 0675	8.210 6989	1.35875	2.3901	6.1467	7·86o

LATITUDE 42°

Lat.	$\log A'$ $\operatorname{diff.} \mathbf{1''} = -0.07$	log B diff. 1"=-0'21	$ \log C $ diff. $\iota'' = + \circ \cdot_{42}$	log I) diff. 1"=+0.00	log E diff. 1"=+0'06	log F diff. 10'=-0'9
0 /					_	
42 00	8.509 0675	8.210 6989	ī·35875	<u>2</u> ·3901 ·	₹.1467	₹.860
I 2	71 66	76 64	900 925	0I 0I	7 I	
	62	51	951	01	74 78	
. 3	58	38	1.35976	02	81	
05 6	54	25	1.36001	02	85	
6	49	12	026	02	89	
7 8	45	8·510 6900 8·510 6887	052 077	03 03	92 96	
9	36	74	102	03	6.1499	
to	8.509 0632	8.210 6861	1.36127	2.3903	6.1203	
11	28	48	152	2 3903	07	
, I2	24	36	178	04	10	
13	19	8·510 6810	203 228	04	14	
14		8.210 6797		04	17	
15 16	07	84	²⁵³ 278	o5 o5	2 I 2 5	
17 18	8.509 0602	72	304	05	25 28	
	8.200 0208	59 46	329	o5 o6	32 .	
19	94		354		35	
20 2I	8.509 0590	8.510 6733	1.36379	2°3906 06	6.1239	7.858
22	85 81	8.510 6707	404 430	06	43 46	
23	77	8.510 6695	. 455	07	50	
24	72	82	480	07	54	
25	68	69	505	07	57 61	
26 27	64	56 43	530 556	o 7 o8	64	
27 28	55	31 18	581	08	68	
29	51	18	606	0.8	72	
30	8.509 0547	8.510 6605	1.36631	2.3908	6.1575	
31	43 38	8.510 6592	656	08		
32	38	79 66	682 707	09 09	79 83 86	
33 34	30	54	732	09	90	
	25	41	757	09	93	
35 36	21	28	757 782	10	6.1292	
37 38	17	8·510 6502	808 822	10 10	6°1601 - 04	
39	08	8.210 6490	833 858	10	08	
40	8.509 0504	8.510 6477	1.36883	2.3910	6.1915	7.856
41	8.200 0200	64	908	ΙΙ	15	, , , ,
42	8.200 0496	51	934	11	19	
43 44	91 87	51 38 25	9 5 9 1 °36984	II	22 26	
		13	1.37009	12	30	
45 46	8 ₃ 78	8.210 6400	034	12	33	
47 48	74	8.510 6387	059 085	I 2 I 2	37	
49	. 70	74 61	110	I 2	41 44	
50 51	8.509 0461	8·510 6348 36	1·37135 160	2.3013	6·1648 52	
52	57 53 48	23	185	13	55	
53	48	8·510 6310 8·510 6297	210	13	59 63	
54			² 35 261		66	
55 56 57 58	40 36	84 71	286	14 14	70	
57	31	59	311	14	73	
58	27	46	336 361	14	77 81	
59	23	33				
60	8.509 0419	8.510 6220	1.37386	2.3914	6.1684	. 7·854

LATITUDE 43°

low A / low D low C low D low E									
Lat.	$\log A'$ diff. $\mathbf{r}'' = -0.07$	$\log B$ diff. $\mathbf{r}'' = -0.51$	$\log C$ diff. $1'' = +0.42$	$ \log D $ diff. $\mathbf{r''} = +0.00$	$\log E$ $\dim E$	$\log F$ $\operatorname{diff.} \ \mathfrak{10'} = -\mathfrak{1'0}$			
° / 43 ° 00 1 2	8·509 0419 14 10	8·510 6220 8·510 6207 8·510 6195	7·37386 412 437	2·3914 15 15	₹.1684 88 92	₹.854			
3 4	06 8·509 0401	82 69	462 487	15 15	6·1699				
o5 6 7 8 9	8·509 0397 93 89 84 80	56 43 30 17 8*510 6105	512 537 563 588 613	15 16 16 16 16	6·1703 06 10 14 17				
10 11 12 13 14	8·509 0376 71 67 63 59	8·510 6092 79 66 53 40	1·37638 663 688 713 739	2·3916 16 17 17 17	6·1721 25 28 32 36				
15 16 17 18	54 50 46 41 37	28 15 8·510 6002 8·510 5989 76	764 789 814 839 864	17 17 17 18 18	39 43 47 50 54				
20 21 22 23 24	8·509 0333 29 24 20 16	8·510 5963 50 38 25 8·510 5912	1·37889 915 940 965 1·37990	2°3918 18 18 18	6·1758 61 65 69 72	7 .85 2			
25 26 27 28 29	8·509 0303 8·509 0299 94	8·510 5899 86 73 60 48	1·38015 040 065 091 116	19 19 19 19	76 80 83 87 91				
30 31 32 33 34	8·509 0290 86 82 77 73	8·510 5835 22 8·510 5809 8·510 5796 83	1°38141 166 191 216 241	2·39 1 9 20 20 20 20	6·1795 6·1798 6·1802 06				
35 36 37 38 39	69 64 60 56 52	71 58 45 32 19	266 292 317 342 367	20 20 20 20 20 21	13 17 20 24 28				
40 41 42 43 44	8·509 0247 43 39 34 30	8·510 5706 8·510 5693 81 68 55	1°38392 417 442 467 492	2·392I 2I 2I 2I 2I	6·1831 35 39 42 46	7.850			
45 46 47 48 49	26 22 17 13 09	42 29 16 8·510 5603 8·510 5591	518 543 568 593 618	2I 2I 22 22 22	50 53 57 61 65				
50 51 52 53 54	8·509 0204 8·509 0200 8·509 0196 92 87	8·510 5578 65 52 39 26	1.38643 668 . 693 719 744	2·3922 22 22 22 22	6·1868 72 76 79 83				
55 56 57 58 59	83 79 74 70 66	8°510 5501 8°510 5488 75 62	769 794 819 844 869	22 23 23 23 23 23	87 91 94 6 ·1898 6·1902				
60	8.509 0162	8.510 5449	1.38894	2°3923	6.1902	7.848			

LATITUDE 44°

Lat.	$\log A$ $\text{diff. } \mathbf{1''} = -0.07$	$ \log B $ $ \dim x'' = -0.51 $	$ \log C $ $ \dim x'' = +0.42 $	$diff. \ r'' = +0.00$	$ \log E $ diff. $\mathbf{r}'' = +0.06$	$ \log F \\ \text{diff. } \text{ro'} = -1 $
0 /						
44 00	8.509 0162	8.510 5449	ī·38894	2.3923	. 6.1902	₹.848
I	57	36 23	919	23	09	
3	53 49	8.510 5411	945 970	23 23	13 17	
4	44	8.510 5398	1.38992	23	20	
o <u>5</u>	40	85	1*39020	23	24	
	36	72	045	24	28	
7 8	31 27	59 46	070 095	24 24	31 35	
9	23	33	120	24	39	
IO	8.209 0119	8.210 2320	1.39145	2*3924	6.1943	
11	14	8.210 2307	171	24	46	
12	10	8.210 2292	196	24	50	
13 14	06 8·509 0102	82 69	221 246	24 24	54 58	•
	8.509 0097	56	271	24	61	
15 16		43	296	24	65	
17	93 89	30	321	24	69	
18 19	84 80	18 8:510 5205	346 371	24 25	72 76	
20 21	8·509 0076 72	8.510 5192	1°39396 422	2° 392 5	6·1980 84	7.845
22	67	79 66	447	25	87	
23	63	53	472	25	91	
24	59	40	497	25	95	
25 26	54 50	28 15	522 547	25 25	6·1 999 6·2 002	
	46	8.210 2102	572	25 25	06	
27 28	42	8.210 2089	597	25	IO	
29	37	76	623	25	14	
30	8.209 0033	8.210 2063	1.39648	2.3925	6.5014	
31 32	29 24	50 37	673 698	25 25	21 25	
33	20	25	723 748	25	29	
34	16	8.210 2013		25	32	
35	II	8.510 4999	773 798	25 26	36	
35 36 37 38	07 8·509 0003	86 73	798 823	26 26	40 44	
	8.208 9999	60	823 848	26	47	
39	94	47	873	26	51	
40	8.508 9990	8.510 4935	1.39898	2.3926	6.2055	7.843
41	86 81	22 8 ·51 0 4909	924	26 26	59 62	
42 43	77	8.510 4896	949 974	26 26	66	
44	73	83	1.39999	26	70	
45	69	70 -	1°40024	26	74	
46	64	57	049	26 26	77 81	
47 48	60 56	44 32	074 099	26 26	85	
49	51	19	124	26	89	
50	8.508 9947	8.510 4806	1.40149	2.3926	6.2092	
51	43	8.510 4793	174	26	6.2096	
52	39	80 67	200 225	26 26	6.2100 04	
53 54	34 30	54	250	26	08	
	26	41	275	26	11	
55 56	21	29	300	26	15	
57 58	17 13	16 8·510 4703	325 350	26 2 6	19 23	
59	09	8.510 4690	375	26 26	23 27	
60	8.508 9904	8.510 4677	1.40400	2.3926	6.5130	7.840

LATITUDE 45°

Lat.	$\log A'$ $\text{diff. } i'' = -0.07$	$\log B$ $\dim B'' = -0.51$		$diff. \ i'' = \pm \circ \circ \circ$	log E diff. 1'' = +0.06	
0 /					,	
45 00	8.508 9904	8.510 4677	ΰ40400	2 ·3926		₹.840
I	8.208 9900	64	425	26	34	7 040
2	8.208 9896	51	450	26	34 38	
3			475	26	42	
4	91 87	39 26	501	26	46	
05		13	526	26	49	
o <u>5</u>	83 78	8.210 4600	551	26	53	
	74	8.510 4587	576	26	57	
7 8	70		601	26	61	
9	66	74 61	. 626	26	64	
IO	8.208 9861	8.210 4248	1.40651	2,3956	6.5168	
II	57	36	676	26	72	
I 2	53 48	23	701	26	76 80	
13		8.510 4510	727	26	80	
14	44	8.510 4497	752	26	83	
15	40	84	777	26	87	
16	36	71	802	26	91	
17 18	31	59	827	26	95	
	27	46	852	26	6.2199	
19	23	33	877	26	6.5505	
20	8.508 9818	8.510 4420	1 *40902	2.3926	6.2206	7.838
21	14	8.510 4407	927	26	10	, -55
22	10	8.210 4394	952	26	14	
23	06	81	1.40978	26	18	
24	8.208 9801	68	1.41003	26	21	
25	8.508 9797	56	028	26	25	
25 26		43	053	26 26	29	
	93 88	43 30	078	26	33	
27 28	84	17		26	37	
29	80	8.210 4304	103 128	26	40	
					6	
30	8.508 9776	8.210 4291	1,41123	2.3926	0*2244	
31	71	78 65	178	26 26	40	
32	62	65	203 229	26 26	54	,
33	67 63 58	52 40	254	2.6	6°2244 48 52 56 60	
34						
35 36	54	27	279	26 25	63 67	
30	50	8:510.4201	304	25	71	
37 38	46	8·510 4201 8·510 4188	329 354	25 25	75	
39	41 37	75	354 3 7 9	25 25	73 79	
39		13	3/9	-5		
40	8·508 9733 28	8.510 4162	1°41404	2.3922	6.2283	7.835
41	28	49	429	25	86	
42	24	37	454	25	90	
43	20	24	479	25	94 6°2298	
44	16	8.210 4111	505	25		
45	II	8.510 4098	530	25	6.5305	
46	07	85	555	25	06	
45 46 47 48	8.508 9703	72	555 580	25	09	
	8.508 9698	60	605	25	13	
49	94	47	630	25	17	
50	8.508 9689	8.510 4034	1.41655	2.3922	6.5351	
50 51	85	21	680	25	25	
52	85 81	8.510 4008	° 705	25	2 5 29	
53	77	8.510 3995	731	25	32	
54	72	8·510 3995 82	756	24	36	
	68	69	781	24	40	
55 56	64	57	806	24	44	
50	60	37 44	831	24	44 48	
57 58	55	31	856	24	52	
59	51	18	881	24	55	
60		8.210 3905	1.41906	2*3924	6.2359	7.832

10806°—11——5

LATITUDE 46°

Lat.	log A' diff. i'' = — 0'07	$\log B$ diff. $1'' = -0.21$	$\log C$ diff. $\mathbf{r}'' = + \circ \cdot_{42}$	$ \log D $ diff. $\tau'' = - \circ \circ \circ$	log E diff. 1" = +0.06	$ \frac{\log F}{\text{diff. ro'} = -r} $
0 / 46 00 I 2 3 4	8·508 9647 43 38 34 30	8.510 3905 8.510 3892 79 67 54	ī·41906 931 957 1·41982 1·42007	2·3924 24 24 24 24		7·832
o5 6 7 8 9	25 21 17 13 08	41 28 15 8.510 3802 8.510 3789	032 057 082 107 132	24 23 23 23 23	79 82 86 90 94	٠
10 11 12 13	8·508 9604 8·508 9600 8·508 9595 91 87	8·510 3776 64 51 38 25	1°42157 183 208 233 258	2·3923 23 23 23 23	6·2398 6·2 402 06 09 13	
15 16 17 18	83 78 74 70 65	8·510 3712 8·510 3699 86 74 61	283 308 333 358 384	23 23 22 22 22	17 21 25 29 33	
20 21 22 23 24	8·508 9561 57 53 48 44	8·510 3648 35 22 8·510 3609 8·510 3596	1·42409 434 459 484 509	2°3922 22 22 22 22	6°2436 40 44 48 52	7.830
25 26 27 28 29	40 35 31 27 23	84 71 58 45 32	534 559 584 610 635	22 21 21 21 21	56 60 64 67 71	
30 31 32 33 34	8·508 9518 14 10 05 8·508 9501	8.510 3519 8.510 3506 8.510 3494 81 68	1·42660 685 710 735 760	2·3921 21 21 21 20	6·2475 79 83 87 91	
35 36 37 38 39	8*508 9497 93 88 84 80	55 42 29 17 8·510 3404	786 811 836 861 886	20 20 20 20 20	95 6·2499 6·2502 06 10	
40 41 42 43 44	8·508 9475 71 67 63 58	8·510 3391 78 65 52 39	1°42911 936 961 1°42987 1°43012	2·3920 19 · 19 19	6·2514 18 22 26 30	7.827
45 46 47 48 49	54 50 45 41 37	27 14 8·510 3301 8·510 3288 75	037 062 087 112 137	19 19 18 18	34 38 41 45 49	
50 51 52 53 54	8·508 9433 28 24 20 16	8·510 3262 49 37 24 8·510 3211	1.43163 188 213 238 263	2°3918 18 18 18	6·2553 57 61 65 69	
55 56 57 58 59	8·508 9403 8·508 9398 94	8·510 3198 85 72 60 47	288 314 339 364 389	17 17 17 17	73 77 81 84 88	
60	8.208 9390	8.510 3134	1.43414	2.3914	6.2592	7.824

LATITUDE 47°

Lat.	$\log A'$ $\operatorname{diff.} \ \mathbf{i''} = -\circ \circ 7$	$diff. \ \mathbf{r''} = - \circ \cdot 2\mathbf{r}$	$\log C$ diff. $\mathbf{r}'' = + \circ \cdot_{42}$	$\log D$ diff, $\mathbf{r}'' = - \circ \circ \circ$	$ \log E $ diff. $\mathbf{r}'' = + \circ \circ \sigma$	$\log F$ $diff. 10' = -1'6$
o / 47 00 I	8·508 9390 86	8.510 3134	ī°43414	2·3917 16	₹.2592 6.5296	= .824
2 3 4	81 77 73	8·510 3108 8·510 3095 82	439 465 490 515	16 16 16	6·2600 04 08	
o5 6 7 8	68 64 60 56 51	70 57 44 31 18	540 565 590 615 641	16 16 15 15	12 16 20 24 28	
10 11 12 13	8·508 9347 43 38 34	8·510 3005 8·510 2993 80 67	1·43666 691 716 741	2·3915 15 14 14	6·2632 35 39 43	
14 15 16 17 18	30 26 21 17 13 09	54 41 28 16 8.510 2903 8.510 2890	766 792 817 842 867 892	14 14 14 13 13	47 51 55 59 63 67	
20 21 22 23 24	8·508 9304 8·508 9300 8·508 9296 91 87	8·510 2877 64 51 39 26	1'43917 943 968 1'43993 1'44018	2°3913 13 12 12	6·2671 75 79 83 87	7.821
25 26 27 28 29	8 ₃ 79 74 70 66	8·510 2800 8·510 2787 74 62	043 069 094 119 144	12 12 11 11	91 95 6·2699 6·2702 06	
30 31 32 33 34	8·508 9261 57 · 53 49 44	8·510 2749 36 23 8·510 2710 8·510 2698	1°44169 195 220 245 270	· 2.3911 10 10	6·2710 14 18 22 26	
35 36 37 38 39	40 36 32 27 23	85 72 59 46 33	295 321 346 3 71 396	10 09 09	30 34 38 42 46	
40 41 42 43 44	8.508 9219 14 10 06 8.508 9202	8·510 2621 8·510 2608 8·510 2595 82 69	1°44421 447 472 497 522	2°3909 08 08 08	6°2750 54 58 62 66	7.817
45 46 47 48 49	8·508 9197 93 89 84 80	57 44 31 18 8·510 2505	547 573 598 . 623 648	07 07 07 07 07	70 74 78 82 86	
50 51 52 53 54	8·508 9176 72 67 63 59	8·510 2493 80 67 54 41	1 ·44673 699 724 749 774	2°3906 06 06 06 05	6°2790 94 6°2798 6°2802 06	
55 56 57 58 59	55 50 46 42 38	28 16 8·510 2403 8·510 2390 77	800 825 850 875 900	05 05 05 04 04	10 14 18 22 26	
60	8.208 9133	8.510 2364	1.44926	2°3904	6.5830	7.814

LATITUDE 48°

Lat.	-	$\log B$ $\operatorname{diff.} \mathbf{i''} = -\circ \cdot 2\mathbf{i}$	$\log C$ diff. $\mathbf{r''} = +0.42$	$ \frac{\log D}{\log D} $	$\log E$ diff. $I'' = + 0.07$	$ \frac{\log F}{\dim F} = -1^{\bullet} $
0 / 48 00 I 2 3 4	8·508 9133 29 25 20 16	8·510 2364 52 39 26 13	ī·44926 951 1·44976 1·45001	2·3904 04 03 03 03	₹.2830 34 38 42 46	₹.814
°5 6 7 8 9	8·508 9103 8·508 9099 95	8.510 2300 8.510 2288 75 62 49	052 077 102 128 153	02 02 02 02 02	50 54 58 62 66	
10 11 12 13	8·508 9091 86 82 78 74	8·510 2236 24 8·510 2211 8·510 2198 85	1.45178 203 229 254 279	2°3901 01 00 00	6·2870 74 78 82 86	
15 16 17 18	69 65 61 57 52	72 60 47 34 21	304 330 355 380 406	2°3900 2°3899 99 99	90 94 6·2898 6·2902 06	
20	8.508 9048	8.510 2108	1°45431	2°3898	6·2910	7.811
21	44	8.510 2096	456	98	14	
22	39	83	481	98	18	
23	35	70	507	97	22	
24	31	57	532	97	26	
25	27	45	557	97	30	
26	22	32	582	97	34	
27	18	19	608	96	38	
28	14	8.510 2006	633	96	42	
29	10	8.510 1993	658	96	46	
30	8.508 9005	8.510 1981	1.45683	2·3 ⁸ 95	6·2950	
31	8.508 9001	68	709	95	54	
32	8.508 8997	55	734	95	58	
33	93	42	759	95	62	
34	88	30	785	94	66	
35	84	17	810	94	70	
36	80	8·510 1904	835	94	74	
37	76	8·510 1891	861	93	78	
38	71	78	886	93	82	
39	67	66	911	93	86	
40 41 42 43 44	8·508 8963 59 54 50 46	8.510 1853 40 27 15 8.510 1802	1°45937 . 962 1°45987 1°46012 038	2°3892 92 91 91	6°2990 94 6°2998 6°3002 06	7.807
45	41	8·510 1789	063	91	10	
46	37	76	088	90	15	
47	33	64	114	90	19	
48	29	51	139	90	23	
49	24	38	164	89	27	
50	8·508 8920	8.510 1725	1·46190	2·3889	6·3031	
51	16	13	215	89	35	
52	12	8.510 1700	240	88	39	
53	08	8.510 1687	266	88	43	
54	8·508 8903	74	291	88	47	
55	8·508 8899	62	316	87	51	
56	95	49	342	87	55	
57	90	36	367	87	59	
58	86	23	392	86	63	
59	82	8.510 1610	418	86	67	
60	8.508 8878	8.210 1298	1.46443	2.3886	6.3041	7.804

LATITUDE 49°

Lat.	log A' diff. I'' = 0'07	log B diff, 1" = -0.21	$\log C$ diff. $\mathbf{1''} = +0.42$	$ \log D $ diff. $\mathbf{r}'' = -\mathbf{o}$ 'or	$\log E$ $diff. i'' = + 0.07$	$\log F$ diff. $10' = -1$
o / 49 00 I 2	8·508 8878 73 69	8·510 1598 85	ī·46443 468	2·3886 85 85	₹.3071 75	₹·804
3 4	65 61	72 59 47	494 519 544	85 84	79 84 88	
05 6 7 8	57 52 48 44 39	34 21 8.510 1508 8.510 1496 83	570 595 621 646 671	84 84 83 83 83	92 6·3096 6·3100 04 08	
10 11 12 13	8.508 8835 31 27 23 18	8.510 1470 58 45 32 19	1°46696 722 747 773 798	2·3882 82 81 81 81	6·3112 16 20 24 28	
15 16 17 18	14 10 06 8.508 8801 8.508 8797	8·510 1407 8·510 1394 81 68 56	824 849 874 899 925	80 80 80 79 79	32 37 41 45 49	
20 21 22 23 24	8·508 8793 89 84 80 76	8.510 1343 30 17 8.510 1305 8.510 1292	1.46950 1.46976 1.47001 026 052	2·3878 78 78 77 77	6°3153 57 61 65 69	7.800
25 26 27 28 29	72 67 63 59 55	79 67 54 41 28	077 103 128 153 179	77 76 76 75 75	73 78 82 86 90	
30 31 32 33 34	8.508 8750 46 42 38 33	8.510 1216 8.510 1203 8.510 1190 78 65	1 ·47204 230 255 281 306	2·3 ⁸ 75 74 74 73 73	6·3194 6·3198 6·3202 06 10	
35 36 37 38 39	29 25 21 16 12	52 39 27 14 8.510 1101	331 357 382 408 433	73 72 72 71 71	15 19 23 27 31	
40 41 42 43 44	8·508 8708 04 8·508 8700 8·508 8695 91	8.510 1088 76 63 50 38	1°47459 484 509 535 560	2·3871 70 70 69 69	6·3235 39 43 47 52	7.796
45 46 47 48 49	87 83 78 74 70	25 12 8.510 1000 8.510 0987 74	586 611 637 662 688	69 68 68 67 67	56 60 64 68 72	
50 51 52 53 54	8·508 8666 61 57 53 49	8·510 0962 49 36 23 8·510 0911	1°47713 738 764 789 815	2°3866 66 66 65 65	6·3276 81 85 89 93	
55 56 57 58 59	45 40 36 32 28	8·510 0898 85 73 60 48	840 866 891 917 942	64 64 63 63 63	6·3297 6·3301 05 09	
60	8.508 8623	8.510 0835	1.47968	2°3862	6.3318	7.792

COAST AND GEODETIC SURVEY.

LATITUDE 50°

Lat.	$ \log A' $ diff. $\mathbf{i''} = -\circ \circ_{7}$	log B diff. 1" = -0'21	$ \log C $ diff. $\mathbf{r''} = + \circ \cdot_{43}$	$ \begin{array}{c} \log D \\ \dim u'' = -o \cdot o u \end{array} $	log E diff. 1" = +0.07	log F diff. 10' = -2'0
0 / 50 00 . I 2 3 4	8·508 8623 19 15 11 06	8·510 0835 22 8·510 0809 8·510 0797 84	ī ·47968 i ·47993 i·48019 044 070	3 .3862 62 61 61 60	₹ 3318 22 26 30 34	7 .792
05	8·508 8602	7 I	095	60	39	
6	8·508 8598	59	121	60	43	
7	94	46	146	59	47	
8	90	33	172	59	51	
9	85	21	197	58	55	
10 11 12 13 14	8·508 8581 77 73 68 64 60	8·510 0708 8·510 0695 83 70 57	1·48223 248 274 299 325 350	2·3858 57 57 56 56 56	6·3359 63 68 72 76 80	
16	56	32	376	55	84	
17	52	19	401	55	88	
18	47	8*510 0607	427	54	93	
19	43	8*510 0594	452	54	6.3397	
20	8·508 8539	8·510 0581	1·48478	2·3 ⁸ 53	6·3401	7°788
21	35	69	504	53	05	
22	30	56	529	5 ²	09	
23	26	43	55 5	52	14	
24	22	31	580	51	18	
25	18	18	606	51	22	
26	14	8·510 0505	631	50	26	
27	09	8·510 0493	657	50	30	
28	05	80	682	49	34	
29	8·508 8501	67	708	49	39	
30	8·508 8497	8·510 0455	1.48734	·2·3 ⁸ 48	6·3443	
31	93	4 ²	759	48	47	
32	88	29	785	47	51	
33	84	17	810	47	55	
34	80	8·510 0404	836	46	60	
35	76	8·510 0392	861	46	64	
36	71	79	887	45	68	
37	67	66	913	45	72	
38	63	54	938	44	76	
39	59	41	964	44	8,1	
40	8·508 8455	8.510 0328	1°48989	2·3843	6·3485	7.784
41	50	16	1°49015	43	89	
42	46	8.510 0303	041	42	93	
43	42	8.510 0291	066	42	6·3497	
44	38	78	092	41	6·3502	
45	34	65	117	41	06	
46	29	53	143	40	10	
47	25	40	169	40	14	
48	21	27	194	39	18	
49	17	15	220	39	23	
50 51 52 53 54	8·508 8413 08 04 8·508 8400 8·508 8396	8.510 0202 8.510 0190 77 64 52	1 ·49246 27 I 297 322 348	2·3838 38 37 37 37 36	6·3527 31 35 40 44	
55	92	39	374	36	48	
56	87	27	399	35	52	
57	83	14	. 425	3 5	56	
58	79	8·510 0101	451	34	61	
59	75	8·510 0089	476	34	65	
60	8.508 8371	8.510 0076	1.49202	2.3833	6.3269	7.780

LATITUDE 51°

Lat.	log A' diff. 1'' = -0'07	log B diff. 1" = -0'21	$\log C$ $\dim C = + o.43$	$ \begin{array}{c} \log D \\ \dim T' = - \circ \circ T \end{array} $	$ \log E $ diff. $\mathbf{i''} = + \circ \circ_7$	log F diff. 10' = - 2'2
o / 51 00 I 2 3 4	8·508 8371 66 62 58 54	8·510 0076 64 51 38 26	T·49502 528 553 579 605	2·3833 33 32 32 31	₹-3569 73 78 82 86	₹.780
o5 6 7 8 9	50 45 41 37 33	8·510 0001 8·509 9988 75 63	630 656 682 707 733	31 30 29 29 28	90 95 6·3599 6·3603 07	
10 11 12 13	8· 5 08 8329 24 20 16 12	8·509 9950 38 25 13 8·509 9900	1°49759 785 810 836 862	2°3828 27 27 26 26	6°3612 16 · 20 24 28	
15 16 17 18	08 8·508 8303 8·508 8299 95 91	8·509 9887 75 62 50 37	887 913 939 965 1*49990	25 25 24 23 23	33 37 41 45 50	
20 21 22 23 24	8.508 8287 82 78 74 70	8·509 9825 8·509 9812 8·509 9799 87 74	1·50016 042 067 093 119	2°3822 22 21 21 20	6*3654 58 63 67 71	7.776
25 26 27 28 29	56 62 57 53 49	62 49 37 24 8·509 9711	145 170 . 196 222 248	20 19 18 18	75 80 84 88 92	
30 31 32 33 34	8·508 8245 41 36 32 28	8·509 9699 86 74 61 49	1.50273 299 325 351 376	2·3817 16 16 15 14	6°3697 6°3 7 01 05 10 14	
35 36 37 38 39	24 20 16 11 07	36 24 8·509 9611 8·509 9599 86	402 428 454 480 505	14 13 13 12	18 22 27 31 35	
40 41 42 43 44	8·508 8203 8·508 8199 95 90 86	8°509 9574 61 48 36 23	1·50531 557 583 609 634	2.3811 10 09 08	6·3740 44 48 52 57	7.772
45 46 47 48 49	82 78 74 70 65	8·509 9511 8·509 9498 86 73 61	660 686 712 738 764	08 07 07 06 05	61 65 70 74 78	
50 51 52 53 54	8·508 8161 57 53 49 45	8·509 9448 36 23 8·509 9411 8·509 9398	1°50789 815 841 867 893	2°3805 04 04 03 02	6·3782 87 91 6·3795 6·3800	
55 56 57 58 59	40 36 32 28 24	86 73 61 48 36	919 944 970 1°50996 1°51022	02 01 01 2·3800 2·3799	04 08 13 17 21	
60	8.508 8120	8.509 9323	1.51048	2.3799	6.3826	7.767

LATITUDE 52°

Lat.	$\log A'$ $\operatorname{diff.} \mathbf{r''} = - \circ^{i} \circ 7$	$\log B$ $diff. r'' = -0.51$	$\log C$ diff. $\mathbf{r''} = +0.43$	$diff. \ i'' = -o.oi$	$\log E$ diff. $\mathbf{r}'' = + \circ \circ 0$	$\log F$ $\dim F \cdot \sigma' = -2^{\circ}3$
o / 52 00 I 2 3 4	8·508 8120 15 11 07 8·508 8103	8·509 9323 8·509 9311 8·509 9298 86 73	T°51048 074 100 126 151	2·3799 98 97 97 96	ē·3826 30 34 39 43	7.767
o5	8·508 8099	61	177	96	47	
6	95	48	203	95	52	
7	90	36	229	94	56	
8	86	23	255	94	60	
9	82	8·509 9211	281	93	65	
10 11 12 13	8·508 8078 74 70 65 61	8·509 9198 86 73 61 48	1.51307 333 359 385 411	2°3792 92 91 91 90	6·3869 73 78 82 86	
15 16 17 18	57 53 49 45 41	36 23 8·509 9111 8·509 9099 86	436 462 488 514 540	89 88 88 87 87	9 1 9 5 6·3899 6·3904 08	
20	8·508 8036	8·509 9074	1·51566	2°3786	6·3912	7.763
21	3 ²	61	592	85	17	
22	28	49	618	85	21	
23	24	36	644	84	25	
24	20	24	670	83	30	
25	16	8·509 9011	696	83	34	
26	11	8·509 8999	722	82	38	
27	07	86	748	81	43	
28	8·508 8003	74	774	81	47	
29	8·508 7999	62	800	80	51	
30	8·508 7995	8·509 8949	1 · 5 1 8 2 6	2·3779	6·3956	
31	91	37	8 5 2	79	60	
32	87	24	8 7 8	78	65	
33	82	8·509 8912	9 0 4	78	69	
34	78	8·509 8899	9 3 0	77	73	
35	74	87	956	76	78	
36	70	74	1·51982	75	82	
37	66	62	1·52008	75	86	
38	62	50	034	74	91	
39	58	37	060	73	6·3995	
40	8·508 7953	·8·509 8825	1·52086	2·3773	6·4000	7.758
41	49	12	112	72	04	
42	45	8·509 8800	138	71	08	
43	41	8·509 8788	164	71	13	
44	37	75	190	70	17	
45 46 47 48 49	33 29 24 20 16	63 50 38 25	216 242 268 294 320	69 68 68 67 66	21 26 30 35 39	
50	8·508 7912	8·509 8701	1 '52347	2°3766	6·4043	
51	08	8·509 8688	373	65	48	
52	04	76	399	64	52	
53	8·508 7900	63	425	64	57	
54	8·508 7895	51	451	63	61	
55	91	39	477	62	65	
56	87	26	503	61	70	
57	83	14	529	61	74	
58	79	8·509 8602	555	60	79	
59	75	8·509 8589	581	59	83	
60	8.508 7871	8.509 8577	1.2608	2.3759	6.4088	7.753

LATITUDE 53°

Lat.	$\log A'$ diff. $\mathbf{r}'' = -0.07$	$\log B$ diff. $r'' = -o^2 I$	$\log C$ diff. $\mathbf{r}'' = + \circ \cdot_{44}$	$\log D$ diff. $\mathbf{r}'' = -\mathbf{o} \cdot \mathbf{o} \mathbf{r}$	$\log E$ diff. $r'' = + o \cdot o_7$	$\log F$ $\dim F = -2$
0 /						
53 00	8.508 7871	8.509 8577	ī·52608	2·3759	€.4088	₹.753
I	67	64	634	58	92	
3	62 58	52 40	660 686	57 56	6·4096 6·4101	
4	54	27	712	56	05	
05 6	50	. 15	738	55	10	
	46	8.509 8502	764	54	14 18	
7 8	42 38	8·509 8490 78	790 817	53 53	23	
9	34	65	843	52	27	
10	8.508 7829	8.509 8453	1.2869	2.3721	6.4132	
11	25	41	895	51	36	
12	21	28 16	921	50.	41	
13 14	17	8.509 8404	94 7 1.52974	49 48	45 49	
15	09	8.509 8391	1.23000	48	54	
16	05	79	026	47	58	
17 18	8.508 7801	67	052	46	63	
19	8·508 7797 92	54 42	078 105	45 45	67 72	
20	8.508 7788	8.509 8329	1.23131	2°3744	6.4176	7.748
21	84	17	157	43	Šo.	7 7 4~
22	80	8.509 8305	183	42	85	
23 24	76 72	8·509 8292 80	209 236	42 41	89 94	
25	68	68	262	40	6.4198	
26	64	55	288	39	6.4203	
27 28	60	43	314	39 38	^C 7	
29	55 51	31 18	341 367	37	12 16	
30	8.508 7747	8.509 8206	1.23393	2*3736	6.4221	
31	43	8·509 8194 82	419	36	25	
32	39	82	446	35	29	
33 34	35 31	69 57	472 498	34 33	34 38	
	27	45	524	33	43	
35 36	23 18	32	551	32	47	
37 38	18 14	8·509 8108	57 7 603	31	52 56	
39	10	8.209 8095	630	30 29	61	
40	8.508 7706	8.509 8083	1.23656	2°372 9	6.4265	7.743
4 I	8.208 7702	71 58	682	28	70	
42	8.208 7698	58	709	27	74	
43 44	94 90	46 34	735 761	26 26	79 83	
	86	22	788	25	88	
45 46	82	8.209 8009	814	24	92	
47 48	77	8.509 7997	840 867	23 22	6·4297 6·4301	
49	73 69	8 ₅ 7 ²	893	22	06	
50	8.508 7665	8•509 7960	1.23919	2.3721	6.4310	
5 I 52	61	48	, 946	20	15	
52	57	36	972	19 18	19	
53 54	53 49	23 8·509 7911	1.23998 1.24022	18	24 28	
	45	8.509 7899	051	17	33	
55 56 57 58	41	87	077	16	37	
57	37	74 62	104	15	42 46	
58 59	32 28	50	130 157	14 14	51	
60	8.508 7624	8.509 7838	1.54183	2.3713	6.4355	7:738

LATITUDE 54°

Lat.	log A' diff. 1''= -0'07	log B diff. 1"=-0'20		$\log D$ diff. $\mathbf{1''} = -0$ or	log E diff. 1"=+0°08	log F diff. 10'= - 2.6
o / 54 00 I 2 3 4	. 8·508 7624 20 16 12 08	8·509 7838 25 13 8·509 7801 8·509 7789	T· 54183 209 236 262 288	2·3713 12 11 10 09	6·4355 60 64 69 73	₹.738
05 6 7 8 9	8·508 7600 8·508 7596 92 88	76 64 52 40 27	315 341 368 394 421	09 08 07 06 05	78 82 87 91 6•4396	
10 11 12 13	8·508 7584 79 75 71 67	8·509 7715 8·509 7703 8·509 7691 78 66	1°54447 474 500 527 553	2°3705 04 03 02 01	6·4400 05 09 14 18	
15 16 17 18	63 59 55 51 47	54 42 30 17 8·509 7605	580 606 633 659 686	00 2°3700 2°3699 98 97	23 28 32 37 41	
20	8·508 7543	8·509 7593	1°54712	2·3696	6·4446	7°733
21	39	81	739	95	50	
22	35	69	765	94	55	
23	31	56	792	94	59	
24	27	44	818	93	64	
25	22	32	845	92	68	
26	18	20	871	91	73	
27	14	8·509 7508	898	90	78	
28	10	8·509 7495	924	89	82	
29	06	83	951	88 .	87	
30	8.508 7502	8·509 7471	1°54977	2·3688	6·4491	
31	8.508 7498	59	1°55004	87	6·4496	
32	94	47	031	86	6·4500	
33	90	34	057	85	05	
34	86	22	084	84	09	
35	82	8·509 7410	110	83	14	
36	78	8·509 7398	137	82	19	
37	74	86	163	82	23	
38	70	74	190	81	28	
39	66	61	217	80	32	
40	8·508 7462	8·509 7349	1.55243	2°3679	6·4537	7 ·72 8
41	58	37	270	78	41	
42	53	25	297	77	46	
43	49	13	323	76	51	
44	45	8·509 7301	350	75	55	
45	. 4I	8·509 7289	376	74	60	
46	37	76	403	74	64	
47	33	64	430	73	69	
48	29	52	456	72	74	
49	25	40	483	71	78	
50 51 52 53 54	8.508 7421 17 13 09	8·509 7228 16 8·509 7204 8·509 7191 79	1°55510 536 563 590 616	2°3670 69 68 67 66	6°4583 87 92 6°4597 6°4601	
55	8°508 7401	67	643	66	06	
56	8°508 7397	55	670	65	10	
57	93	43	696	64	15	
58	89	31	723	63	20	
59	85	19	750	62	24	
60	8.508 7381	8.509 7107	1.55777	2.3661	6°4629	7.723

LATITUDE 55°

	diff. $1'' = -0.07$	diff. i'' = -o'20	diff. $r'' = +0.45$	$diff. i'' = -o^*o_2$	diff. 1" = +0.08	diff. $10' = -2$
0 /						
55 00	8·508 7 381	8.509 7107	ī·55777	2 ·3661	= .4629	7.723
I	77	8.509 7095	803	60		, , 3
2	73	82	830	59 58	33 3 8	
3	69	70	857		43	
4	65	58	884	57	47	
05 6	61	46	910	56	52	
	56	34	937	56	57	
7 8	52 48	8·509 7010	964 1 .25991	55 54	61 66	
9	44	8.209 6998	1.26014	53	70	
*0						
10 11	8°508 7340 36	8.509 6986	1°56044 071	2°3652 51	6·4675 80	
12	32	74 62	098	50	. 84	
13	28	49	125	49	89	
14	24	37	151	48	94	
15	20	25	178	47	6.4698	
16	16	13	205	46	6.4703	
17 18	12	8.209 6901	232	45	08	
	08	8.509 6889	259 286	44	12	
19	04	77	200	43	17	
20	8.508 7300	8.509 6865	1.26315	2.3642	6.4721	7.717
21	8.508 7296	53	339	42	26	
22	92 88	41	366	41	31	
23 24	84	29 17	393 420	40 3 9	3 5 40	
		•				
25 26	80 76	8·509 6805 8·509 6793	447	38	4 5 4 9	
	70 72	81	474 500	3 7 36	5 ‡	
27 28	68	69	527	35	59	
29	64	57	554	34	59 63	
30	8.508 7260	8.509 6745	1.26581	2.3633	6 ·4768	
31	56	33	008	32		
32	52 48	21	635 662	3 I	73 77 82	
33		8.509 6709	662	30	82	
34	44	8.509 6696	689	29	87	
35 36	40	84	716	28	91	
36	36	72 60	743 770	27 2 6	6·4796 6·4801	
37 38	32 28	48	797	25	05	
39	24	36	823	24	10	
	8.508 7220	8.509 6624	1.26820	2.3623	6.4812	7.711
40 41	16	I 2	877	2 3023	20	/ /
42	12	8.509 6600	904	21	24	
43	o8	8.509 6588	931	20	29	
44	04	76	958	19	34	
45	8.508 7200	64	1.26982	18	38 43 48	
45 46	8.508 7196	52	1.24015	17	43	
47 48	92 88	40 28	039 066	16	48	
48 49	. 84	28 16	093	15 14	52 57	
49						
50	8.208 7180	8.509 6505	1.27120	2.3613	6.4862	
51	76	8·509 6493 81	147	I 2 I I	66 71	
52	72 68	69	174 201	10	76	
53 54	64	57	229	09	76 81	
	60	45	256	08	85	
55 56	56	33	283	07	90	
57	52	21	310	06	6.4892	
57 58	5 ² 48	8.509 6409	337	05	6.4900	
59	44	8.509 6397	364	04	04	
	8.508 7140	8.509 6385	1,24391	2*3603	6.4909	7.706

LATITUDE 56°

Lat.	log A' diff. 1" = -0'07	log B diff. 1"=-0.20	log C diff. 1" = +0.45	log D diff. 1'' = -0'02	$\log E$ diff. $\mathbf{r}'' = + \circ \circ 8$	$\log F$ diff. $10' = -3$ 'o
0 /						
56 00 I 2 3	8·508 7140 36 32 28 24	8·509 6385 73 61 49 37	ī·57 391 418 445 472	2·3603 02 01 2·3600	ē∙4909 14 · 18 23 28	₹.706
4 05 6 7 8 9	20 16 12 08 04	25 13 8·509 6301 8·509 6289 77	499 526 554 581 608 635	2°3599 98 97 96 95 94	33 37 42 47 52	
10	8.508 7100	8.509 6266	1.57662	2°3593	6°4956	
11	8.508 7096	54	689	92	61	
12	92	42	717	91	66	
13	88	30	744	90	71	
14	84	18	771	89	75	
15 16 17 18	80 76 72 69 65	8·509 6206 8·509 6194 82 70 58	798 82 5 852 880 907	88 87 86 85 84	80 85 90 94 6•4999	
20	8·508 7061	8·509 6147	1·57934	2·3583	6·5004	7.700
21	57	35	961	82	09	
22	53	23	1·57989	81	13	
23	49	8·509 6111	1·58016	80	18	
24	45	8·509 6099	043	78	23	
25	41	87	070	77	28	
26	37	75	098	76	32	
27	33	63	125	75	37	
28	29	51	152	74	42	
29	25	40	179	73	47	
30	8·508 7021	8·509 6028	1.58207	2°3572	6·5052	
31	17	16	234	71	56	
32	13	8·509 6004	261	70	61	
33	09	8·509 5992	289	69	66	
34	05	80	316	68	71	
35	8·508 7001	68	343	67	75	
36	8·508 6997	57	371	66	80	
37	93	45	398	65	85	
38	89	33	425	64	90	
39	86	21	453	62	95	
40	8·508 6982	8·509 5909	1·58480	2°3561	6·5099	7.694
41	78	8·509 5897	507	60	6·5104	
42	74	86	535	59	09	
43	70	74	562	58	14	
44	66	62	589	57	19	
45	62	50	617	56	24	
46	58	38	644	55	28	
47	54	2 7	672	54	33	
48	50	15	699	53	38	
49	46	8·509 5803	726	52	43	
50	8·508 6942	8·509 5791	1°58754	2°3550	6·5148	
51	38	79	781	49	52	
52	34	67	809	48	57	
53	30	56	836	47	62	
54	26	44	864	46	67	
55	23	32	891	45	72	
56	19	20	919	44	77	
57	15	8·509 5709	946	43	81	
58	11	8·509 5697	1·58974	42	86	
59	07	85	1·59001	41	91	
60	8.508 6903	8.509 5673	1.59028	2.3539	6.2196	7.688

LATITUDE 57°

Lat.	diff. i'' = - o'o6	log B	$ \log C $ $ \dim T'' = + 0.46 $	$\log D$ $\dim T'' = -o \cdot o $	$\log E$ diff, $r'' = + o \cdot o 8$	$\log F$ diff. $10' = -3$
o / 57 00	8.508 6903	8.509 5673	ī·59028			7 .688
I	8.208 6899	61	056	2 *3539 38	6.201	7.000
2	95	50	083	37	06	
3 4	91 87	38 26	111	36 35	10 15	
	83	14	166	34	20	
0 5 6	79	8.509 5603	194	33	25	
7 8	75	8.509 5591	221	32	30	
9	72 68	79 67	249 276	30 29	35 40	
10	8.508 6864	8.509 5556	1.59304	2*3528 .	6.5244	
ΙΙ	60	44	331	27	49	
12	56 52	32 20	359 387	26 25	54	
14	48	8.509 5509	414	25 24	59 64	
15	44	8.509 5497	442	22	69	
16 17	40 36	85	469 497	2 I 20	74	
17 18	32	73 62	525	19	79 83 3 8	
19	28	50	552	ıŚ	88	
20	8.508 6825	8.509 5438	1.59580	2.3212	6.5293	7.682
2 I 22	21	27 15	608 635	16 14	6·5298 6·5303	
23	13	8.509 5403	663	13	08	
24	09	8.509 5392	691	I 2	13	
25 26	05 8·508 6801	80 68	718 746	1 i	18 22	
27 28	8.508 6797	56	774	09	27 27	
28 29	93	45	801 829	07	32	
	90	33		06	37	
30 31	8·508 6786 82	8·509 5321 8·509 5310	1.29824 882	2·3505 04	6·5342 47	
32	78	8.209 2298	912	03	52	
33 34	74 70	86 75	940 968	02	57 62	
	66	63	1.29996	2·3500 2·3499	67	
35 36 37 38	62	51	1.60023	98	72	
37 38	58 54	40 28	05 I 079	97 96	76 81	
39	51	16	107	95	86	
40	8.508 6747	8.509 5205	1.60134	2.3493	6.2391	7 ·675
4 I	43	8:509 5193	162	92	6.5396	, -13
42 43	39 35		190 218	9 1 90	6 · 5401 06	
44	31	70 58	246	89	11	
45	27	. 46	274	87	16	
46 47	23	35 23	301 329	86 8 5	21 26	
47 48	16	I 2	357	8 5 84	31	
49	12	8.209 2100	385	83	36	
50	8.508 6708	8.509 5088	1.60413	2°3481 80	6.5441	
51 52	8· 5 08 6700	77 65	44 1 469		46 50	
53	8.208 6696	54	496	79 78	55 60	
54	92	42	524	76		
55 56 57 58	89 85	30 19	552 580	75 74	65 70	
57	85 81	8.509 5007	608	73	- 75 80	
58	77	8·509 4996 84	636 664	7 2 70	80 85	
59	73					
60	8.208 6669	8.509 4972	1.60692	2.3469	6.2490	7.669

LATITUDE 58°

Lat.	$ \log A' \\ \text{diff. } \mathbf{r}'' = -0.06 $	$ \begin{array}{c} \log B \\ \dim x'' = -0.19 \end{array} $	$ \log C $ diff. $\mathbf{r}'' = + \circ \cdot 47$	$ \log D $ diff. $t'' = -0.02$	$ \log E $ diff. $\mathbf{i}'' = + \circ \cdot \circ 8$	$ \log F $ $ \dim F = -3 $
0 /				•	_	
58 00	8.508 6669	8.509 4972	T ·60692	2 *3469	6 ·5490	₹.669
I	65	61	720	68	6.5495	
3	62 58	49 38	748 776	67 66	6·5500 05	
4	54	26	804	64	10	
o5 6	50	14	832	63	15	
	46	8.509 4903	86o 888	62 61	20	
7 8	42 38	8·509 4891 80	916	59	25 30	
9	35	68	944	58	35	•
IO	8.508 6631	8.509 4857	1.60972	2.3457	6.5540	
II	27	45	1,61000	56	45	
12	23	33	028	54	50	
13 14	19 15	22 8·509 4810	056 084	53 52	55 60	
15	11	8.509 4799	112	51	65	
16	08	87	140 168	49 48	70	
17 18	04 8·508 6600	76 64	197	48 47	75 80	
19	8.508 6596	53	225	46	85	
20	8.508 6592	8·5 0 9 4741	1.61253	2:3444	6.2590	7.662
21	88	30 18	281	43	6.5595	
22 23	85 81	18 8·509 4707	309 337	4 2 41	6 · 5600	
24	77	8.509 4695	337 365	39	10	
25	73	84	393	38	15	
26	69	72	422	37	20	
27 28	65 62	61 40	450 478	35 34	2 5 30	
29	58	49 38	506	34 33	35	
30	8.508 6554	8.509 4626	1.61534	2.3432	6.2640	
31	50	15	563	30	45	
32	46	8:509 4603	591 619	29 . 28	50	
33 34	42 39	8·509 4592 80	647	26 26	55 60	
1	35	69	675	25	65	
35 36	31	57	704	24	70	
37 38	27 23	46 35	73 ² 760	23 21	75 80	
39	20	23	789	20	86	
40	8.508 6516	8.509 4512	1.61817	2.3419	6.2691	7.656
41	12	8.509 4500	845	17	6.5696	
42	08	8.509 4489	873 902	16 15	6·5701 06	
43 44	04 8·508 6500	77 66	930	15	11	
45	8.508 6497	54	958	12	16	
46	93 89	43	1.62015	11	21 26	
47 48	85	32 20	1·62015 043	10 08	. 31	
49	85 81	8.509 4409	072	07	36	
50	8.508 6478	8.509 4397	1.62100	2*3406	6.5741	
51	74	86	I 29	04	46	
5 ² 53	70 66	74 63	157 185	03 02	51 56	
53 54	62	52	214	2.3400	62	
	59	40	242	2*3399	67	
55 56 57 58	55 51 ~	29 17	27 I 299	98 96	72	
58	47	8.509 4306	327	9 5	77 82	
59	43	8.509 4295	356	94	87	
60	8.508 6440	8.509 4283	1.62384	2.3395	6.2455	7.649

LATITUDE 59°

Lat.	log A' diff. 1"=-0.06	log B diff. r"=-o'19	log C diff. 1"=+0.48	$ \begin{array}{c} \log D \\ \dim x'' = -0.02 \end{array} $	log E diff. 1"=+0'09	$ \log F $ diff. $ro' = -3.5$
o / 59 00 I 2 3 4 05 6 7	8·508 6440 36 32 28 24 21 17 13	8·509 4283 72 61 49 38 26 15 8·509 4204 8·509 4192	7·62384 413 441 470 498 527 555 584 612	2·3392 91 90 88 87 86 84 83 82	6.5792 6.5797 6.5802 07 13 18 23 28	₹ ·649
9 10 11 12 13 14 15 16 17 18	8.508 6402 8.508 6398 94 90 87 83 79 75 71 68	81 8.509 4170 58 47 36 24 13 8.509 4102 8.509 4090 79 68	641 1.62669 698 727 755 784 812 841 870 898	80 2°3379 78 76 75 74 72 71 69 68 67	38 6·5843 48 54 59 64 69 74 79 84	
20 21 22 23 24	8·508 6364 60 56 53 49	8·509 4056 45 34 22	1.62955 1.62984 1.63013 041 070	2·3365 64 63 61 60	6.5895 6.5900 05 10	7.642
25 26 27 28 29	45 41 38 34 30	8·509 4000 8·509 3989 77 66 55	099 127 156 185 214	58 57 56 54 53	20 26 31 36 41	
30 31 32 33 34	8.508 6326 23 19 15	8·509 3943 32 21 8·509 3910 8·509 3898	1.63242 271 300 329 357	2°3351 50 49 47 46	6°5946 .51 57 62 67	
35 36 37 38 39	08 04 8·508 6300 8·508 6296 93	87 76 65 53 42	386 415 444 473 501	44 43 42 40 39	72 77 82 88 93	
40 41 42 43 44	8·508 6289 85 81 78 74	8·509 3831 20 8·509 3808 8·509 3797 86	1.63530 559 588 617 646	2·3337 36 35 33 32	6·5998 6·6003 08 14 19	7.635
45 46 47 48 49	70 66 63 59 55	75 63 52 41 30	674 703 732 761 790	30 29 28 26 25	24 29 34 40 45	
50 51 52 53 54	8·508 6251 48 44 40 36	8·509 3719 8·509 3708 8·509 3696 85 74	1.63819 848 877 906 935	2·3323 22 20 19	6·6050 55 61 66 71	
55 56 57 58 59	33 29 25 22 18	63 52 40 29 18	964 1·63993 1·64022 051 080	16 15 13 12 10	76 81 87 92 6·6097	
60	8.508 6214	8.509 3607	1.64109	2*3309	6.6103	7.627

LATITUDE 60°

Lat.	log A' diff. 1''=-0'06	log B diff. 1''=-0'18	log C	log D diff. 1"=-0'03	log E diff. 1''=+0'09	log F diff. 10'=-3'7
o / 6o oo I 2	8·508 6214 10 07 8·508 6203	8·509 3607 8·509 3596 85	ī·64109 138 167 196	2·3309 07 06 04		7 .627
3 4	8.208 6199	73 62	225	03	23	
o <u>5</u>	96	51	254	02	29	
6	92	40	283	2·3300	34	
7	88	29	312	2·3299	39	
8	84	18	341	97	44	
9	81	8·509 3507	370	96	50	
10	8·508 6177	8·509 3495	1·64400	2°3294	6·6155	
11	73	84	429	93	60	
12	70	73	458	91	66	
13	66	62	487	90	71	
14	62	51	516	88	76	
15 16 17 18	58 55 51 47 44	40 29 18 8.509 3407 8.509 3395	545 574 604 633 662	87 85 84 82 81	81 87 92 6·6197 6·6203	
20	8·508 6140	8·509 3384	1·64691	2·3279	6·6208	7.620
21	36	73	720	78	13	
22	33	62	750	76	18	
23	29	51	779	75	24	
24	25	40	808	73	29	
25	21	29	838	72	34	
26	18	18	867	70	40	
27	14	8·509 3307	896	69	45	
28	10	8·509 3296	925	67	50	
29	07	85	955	66	56	
30	8·508 6103	8·509 3274	1.64984	2·3264	6·6261	
31	8·508 6099	63	1.65013	63	66	
32	96	·52	043	61	72	
33	92	40	072	60	77	
34	88	29	101	58	82	
35	85	18	131	57	87	
36	81	8·509 3207	160	55	93	
37	77	8·509 3196	190	54	6·6298	
38	74	85	219	52	6·6304	
39	70	74	248	51	09	
40	8·508 6066	8·509 3163	1.65278	2·3249	6·6314	7.613
41	63	52	307	48	20	
42	59	41	337	46	25	
43	55	30	366	45	30	
44	52	19	396	43	36	
45	48	8·509 3108	425	41	41	
46	44	8·509 3097	455	40	46	
47	41	86	484	38	52	
48	37	75	514	37	57	
49	33	64	543	35	62	
50	8·508 6030	8·509 3053	1.65573	2°3234	6·6 ₃ 68	
51	26	42	602	32	73	
52	22	31	632	31	79	
53	19	20	661	29	84	
54	15	8·509 3010	691	28	89	
55 56 57 58 59	8.508 6000 8.508 5997	8· 5 09 2999 88 77 66 55	721 750 780 809 839	26 24 23 21 20	6.6395 6.6400 05 11 16	
60	8.208 2993	8.509 2944	1.65869	2,3218	6.6422	7.605

L'ATITUDE 61°

Lat.			$\log C$ $diff. \ 1'' = + \circ 50$	log [) diff. 1" = -0'03	$ \log E $ diff. $\mathbf{r}'' = + \circ \circ \circ \circ$	$ \begin{array}{c} \log F \\ \dim ro' = -4^{\circ}c \end{array} $
o / 61 00 1 2 3 4 05 6 7 8	8·508 5993 89 86 82 79 75 71 68 64 60	8·509 2944 33 22 11 8·509 2900 8·509 2889 78 67 56 46	1.65869 898 928 958 1.65987 1.66017 047 076 106 136	2·3218 17 15 13 12 10 09 07 06 04	5.6422 27 32 38 43 48 54 59 65	₹ .605
10 11 12 13 14 15 16 17 18	8.508 5957 53 49 46 42 39 35 31 28 24	8·509 2835 24 13 8·509 2802 8·509 2791 80 69 58 48	1.66166 195 225 255 285 315 344 374 404 434	2·3202 2·3201 2·3199 98 96 94 93 91 90 88	6·6476 81 87 92 6·6497 6·6503 08 14 19 25	
20 21 22 23 24 25 26	17 13 10 06 8.508 5902 8.508 5899	8·509 2726 15 8·509 2704 8·509 2693 83 72 61 50		2·3186 85 83 81 80 78 77 75	6.6530 36 41 46 52 57 63 68	7.597
27 28 29 30 31 32 33 34	95 . 92 . 88 8·508 5884 81 77 74 70	8·509 2618 8·509 2607 8·509 2596 85 74	703 733	2°3170 68 67 65 64	74 79 6·6585 90 6·6596 6·6601	
35 36 37 38 39	66 63 59 56 52	64 53 42 31 20	913 943 1.66973 1.67003 .033	62 60 58 57 55	12 18 23 29 34	7 ·589
40 41 42 43 44 45 46 47	8·508 5848 45 41 38 34 30 27 23	8.509 2510 8.509 2499 88 77 67 56 45 34	1·67063 094 124 154 184 214 244 274	2°3154 52 50 49 47 45 44 42	45 51 56 62 67 73 78	7 309
47 48 49 50 51 52 53 54	8·508 5813 09 05 8·508 5802 8·508 5798	8.509 2402 8.509 2391 81 70 59	305 335 1.67365 395 425 456 486	40 39 2.3137 35 34 32 30	84 89 6.6695 6.6700 06 12	
55 56 57 58 59	95 91 88 84 80	49 38 27 16 8.509 2306	516 547 577 607 637	29 27 25 23 22	23 28 34 39 45	
60	8.508 5777	8.509 2295	1.67668	2.3120	6.6750	7.581

LATITUDE 62°

Lat.		log B diff. 1" = -0.18	$\log C$ $\dim C = + \circ \cdot 51$	log D diff. 1"=-0'03	log E diff. r'' = +0.09	$\log F$ $\dim F = -4$
62 00 I 2 3 4	8·508 5777 73 70 66 63	8·509 2295 84 74 63 · 52	7·67668 698 728 759 789	2·3120 18 17 15 13	6·6750 56 61 67 73	- 7·581
o5	59	42	820	12	78	
6	55	31	850	10	84	
7	52	20	880	08	89	
8	48	8.509 2210	911	06	6·6795	
9	45	8.509 2199	941	05	6·6801	
10	8.508 5741	8·509 2188	1.67972	2°3103	6·6806	
11	38	78	1.68002	01	12	
12	34	67	033	2°3100	17	
13	30	56	063	2°3098	23	
14	27	46	094	96	29	
15 16 17 18	. 24 20 16 . 13 09	35 25 14 8·509 2103 8·509 2093	124 155 185 216 246	94 93 91 89 87	34 40 45 51 57	
20	8·508 5706	8·509 2082	1.6827 7 . 3°7	2·3086	6·6862	7.573
21	8·508 5702	7 1	3°8	84	68	
22	8·508 5699	6 1	38	82	73	
23	95	50	369	80	79	
24	92	40	399	79	85	
25	88	29	430	77	90	
26	85	19	461	75	6*6896	
27	81	8·509 2008	491	74	6:6902	
28	78	8·509 1997	522	72	07	
29	74	87	553	70	13	
30	8·508 5671	8·509 1976	1·68583	2·3068	6·6919	
31	67	66	614	66	24	
32	64	55	645	65	30	
33	60	45	675	63	36	
34	56	34	706	61	41	
35	53	23	737	59	47	
36	49	13	768	58	53	
37	46	8·509 1902	799	56	58	
38	42	8·509 1892	829	54	64	
39	39	81	860	52	70	
40	8.508 5635	8·509 1871	1.68891	2·3050	6·6975	7.564
41	32	60	922	49	81	
42	28	50	953	47	87	
43	25	39	1.68984	45	92	
44	21	29	1.69014	43	6·6998	
45	18	18	045	42	6·7004	
46	14	8·509 1808	076	40	09	
47	11	8·509 1797	107	38	15	
48	07	87	138	36	21	
49	04	76	169	34	26	
50	8·508 5600	8·509 1766	1.69200	2·3033	6·7032	
51	8·508 5597	55	231	31	38	
52	93	45	262	29	44	
53	90	34	293	27	49	
54	86	24	324	25	55	
55 56 57 58 59	83 80 76 73 69	8·509 1703 8·509 1693 82 72	355 386 417 448 479	23 22 20 18 16	61 67 72 78 84	
60	8.508 5566	8.209 1661	1.69210	2.3014	6.7089	7.556

LATITUDE 63°

Lat.	log A' diff. 1'' = -0'06	log B diff. "" = -0"17	$ \frac{\log C}{\dim x'' = + \circ^* 52} $	$\log D$ diff. $t'' = -0.03$	log E diff. 1" = +0'10	
63 00 I 2 3	8·508 5566 62 59 55 52	8·509 1661 51 40 30 20	7·69510 541 572 603 635	2·3014 13 11 09 07	6·7089 6·7095 6·7101 07	7 .556
05	48	8·509 1609	666	. 05	18	
6	45	8·509 1599	697	03	24	
7	41	88	728	02	30	
8	38	78	759	2·3000	35	
9	34	68	791	2·2998	41	
10	8·508 5531	8·509 1557	1.69822	2·2996	6·7147	-
11	27	47	853	94	53	
12	24	36	884	92	59	
13	20	26	915	90	64	
14	17	16	947	89	70	
15 16 17, 18	14 10 07 03 8.508 5500	8·509 1505 8·509 1495 85 74 64	1.69978 1.70009 041 072 103	87 85 83 81 79	76 82 88 93 6•7199	
20	8·508 5496	8·509 1454	1·7013 5	2·2977	6·7205	7.547
21	93	43	166	75	11	
22	89	33	197	74	17	
23	86	23	229	72	22	
24	86	12	260	70	28	
25	79	8·509 1402	292	68	34	
26	76	8·509 1392	323	66	40	
27	72	81	355	64	46	
28	69	71	386	62	51	
29	65	61	417	60	57	
30	8·508 5462	8·509 1350	1·70449	2·2958	6·7263	
31	58	40	480	57	69	
32	55	30	512	55	75	
33	52	19	544	53	81	
34	48	8·509 1309	575	51	86	
35	45	8·509 1299	607	49	92	
36	41	89	638	47	6·7298	
37	38	78	670	45	6·7304	
38	34	68	701	43	10	
39	31	58	733	41	16	
40 41 42 43 44	8·508 5428 24 21 17 14	8·509 1248 37 27 17 8·509 1207	1 ·70765 796 828 860 891	2·2939 37 36 34 32	6·7 ₃₂₂ 28 33 39 45	7.538
45 46 47 48 49	8·508 5400 8·508 5397	8·509 1196 86 76 66 55	923 955 1.70986 1.71018 050	30 28 26 ' 24 22	51 57 63 69 75	
50	8·508 5394	8·509 1145	1.71082	2°2920	6·7381	
51	90	35	114	_ 18	86	
52	87	25	145	_ 16	92	
53	83	15	177	_ 14	6·7398	
54	80	8·509 1104	209	_ 12	6·7404	
55	77	8·509 1094	241	10	10	
56	73	84	273	08	16	
57	70	74	305	06	22	
58	66	64	337	04	28	
59	63	54	368	02	34	
60	8.508 5360	8.509 1043	1.71400	2.5001	6.7440	7.529

LATITUDE 64°

Lat.	$\log A'$ diff. $\mathbf{r''} = - \circ \circ \circ \circ \circ$	$\log B$ diff. $\mathbf{i''} = -0.17$	$\log C$ diff. $\mathbf{i''} = + \circ \cdot 54$	$\log D$ diff. $r'' = -0.03$	log E diff. 1" = +0'10	log F diff. 10' = -4'7
64 00 I 2 · 3 4	8·508 5360 56 53 49 46	8·509 1043 33 23 13 8·509 1003 8·509 0993	7·71400 432 464 496 528	2·2901 2·2899 97 95 93	5·7440 46 52 58 63	. 7 ·529
0 5 6 7 8 9	43 39 36 33 29	6 309 0993 82 72 62 52	592 624 656 688	89 87 85 83	75 81 87 93	
10 11 12 13 14	8·508 5326 22 19 16 12	8·509 0942 32 22 12 8·509 0902 8·509 0891	1.71720 752 785 817 849 881	2·2881 79 77 75 - 73	6·7499 6·7505 11 17 23	
16	06	81	913	69	35	
17	8*508 5302	71	945	67	41	
18	8*508 5299	61	1.71977	6 5	47	
19	96	51	1.72010	63	53	
20	8·508 5292	8·509 0841	1·72042	2·2861	6·7559	7.520
21	89	31	074	59	65	
22	85	21	106	57	71	
23	82	11	139	55	77	
24	79	8·509 0801	171	53	83	
25 26 27 28 29	75 72 69 65 62	8·509 0791 81 71 61 51	203 235 268 300 332	51 49 47 45 42	89 6·7595 6·7601 07	
30	8·508 5259	8·509 0741	1·72365	2·2840	6·7619	
31	55	31	397	38	25	
32	52	21	430	36	31	
33	49	11	462	34	37	
34	45	8·509 0701	495	32	43	
35	42	8·509 0691	527	30	49	
36	39	81	559	28	56	
37	35	71	592	26	· 62	
38	32	61	624	24	68	
39	29	51	657	22	74·	
40 41 42 43 44	8·508 5225 22 19 15	8·509 0641 31 21 11 8·509 0601	1·72689 722 755 787 820	2·2820 18 16 14 12	6·7680 86· 92 6·7698 6·7704	7.511
45	09	8·509 0591	852	10	10	
46	05	81	885	07	16	
47	8·508 5202	71	918	05	22	
48	8·508 5199	61	950	03	28	
49	95	51	1.72983	2·2801	35	
50	8·508 5192	8·509 0541	1.73016	2·2799	6·7741	
51	89	31	048	97	47	
52	86	21	081	95	53	
53	82	11	114	93	59	
54	79	8·509 0501	146	91	65	
55	76	8·509 0491	179	89	71	
56	72	82	212	87	77	
57	69	72	245	84	84	
58	66	62	278	82	90	
59	62	52	310	80	6·7796	
60	8.508 5159	8.509 0442	1.73343	2.2778	6.7802	7.501

LATITUDE 65°

Lat.	$\log A'$ $\text{diff. } \mathbf{i''} = - \text{ o'o5}$	$\log I $ $diff. r'' = - \circ 16$	$\log C$ diff. $\mathbf{r''} = +0.56$	$\log D$ diff. $\mathbf{r}'' = -0.04$	log E diff. r'' = +0'10	$\log F$ diff. $10' = -5$ 0
65 00 I 2 3 4	8·508 5159 56 52 49 46	8·509 0442 32 22 12 8·509 0402	ī·73343 376 409 442 475	2·2778 76 74 72 70		7.501
05	43	8·509 0393	508	68	33	
6	39	83	541	65	39	
7	36	73	574	63	45	
8	33	63	607	61	51	
9	30	53	640	59	57	
10	8.508 5126	8·509 0344	1.73673	2*2757	6·7864	
11	23	34	706	55	70	
12	20	24	739	53	76	
13	17	14	772	50	82	
14	13	8·509 0304	805	48	88	
15 16 17 18	07 03 8.508 5100 8.508 5097	8·509 0295 85 75 65 55	838 871 904 937 1.73970	46 44 42 40 38	6·7895 6·7901 07 13	
20	8·508 5094	8·509 0245	1.74004	2·2735	6·7926	7 ·49 1
21	90	36	037	33	32	
22	87	26	070	31	38	
23	84	16	103	29	44	
24	81	8·509 0206	136	27	51	
25	77	8·509 0197	170	24	57	
26	74	87	203	22	63	
27	71	77	236	20	69	
28	68	67	270	18	76	
29	64	57	303	16	82	
30 31 32 33 34	8·508 5061 58 54 51 48	8·509 0148 38 28 18 8·509 0109	1.74336 370 403 436 470	2·2714 11 09 07 05	6·7988 6·7994 6·8001 07	
35	45	8·509 0099	503	03	19	
36	41	, 89	537	2°2700	26	
37	38	80	570	2°2698	32	
38	35	70	604	96	38	
39	32	60	637	94	44	
40	8·508 5029	8·509 0051	1°74670	2·2692	6·8051	7.481
41	25	4I	704	89	57	
42	22	3I	738	87	63	
43	19	22	771	85	70	
44	16	I2	805	83	76	
45	13	8·509 0002	838	80	82	
.46	09	8·508 9993	872	78	89	
47	06	83	906	76	6·8095	
48	03	73	939	74	6·8101	
49	8.508 5000	64	1.74973	72	07	
50	8·508 4996	8·508 9954	1.75007	2·2669	6·8114	
51	93	44	040	67	20	
52	90	35	074	65	27	
53	87	25	108	63	33	
54	84	15	142	60	39	
55	80	8·508 9906	175	58	46	
56	77	8·508 9896	209	56	52	
57	74	87	243	53	58	
58	71	77	277	51	65	
59	68	67	311	49	71	
60	8.508 4964	8.208 9828	1.75344	2°2647	6.8177	7 .47 I

LATITUDE 66°

Lat.	$\log A'$ diff. $i'' = -o \cdot o_5$	$ \log B $ diff. $\mathbf{r}'' = - \circ 16$	$ \log C $ diff. $\mathbf{r''} = + \circ \cdot 57$	log D diff. 1" = -0'04	$ \log E $ diff. $\mathbf{r}'' = + \mathbf{o}'\mathbf{r}\mathbf{r}$	log F diff. 10'=-5'3
o / 66 oo I 2 3 4	8·508 4964 61 58 55 52	8·508 9858 48 39 29	7·75344 378 412 446 480	2·2647 44 42 40 38	6·8177 84 90 6·8196 6·8203	= 7·47 I
o5 6 7 8	48 45 42 39 36	10 8·508 9801 8·508 9791 82 72	514 548 582 616 650	35 33 31 28 26	09 16 22 28 35	
10	8·508 4933	8·508 9762	1.75684	2·2624	6.8241	٠
11	29	53	718	22	48	
12	26	43	752	19	54	
13	23	34	786	17	61	
14	20	24	820	15	67	
15 16 17 18	17 13 10 07 04	8·508 9705 8·508 9696 86 77	854 889 923 957 1.75991	12 10 08 05 03	73 80 86 93 6·8299	
20	8·508 4901	8·508 9667	1·76025	2°2601	6·8306	7°461
21	8·508 4898	58	060	2°2598	12	
22	95	48	094	96	19	
23	91	39	128	94	25	
24	88	29	163	91	31	
25	85	20	197	89	38	
26	82	11	231	87	44	
27	79	8·508 9601	266	84	51	
28	76	8·508 9592	300	82	57	
29	73	82	334	80	64	
30	8·508 4869	8·508 9573	1.76369	2°2578	6·8 ₃₇ 0	
31	66	63	403	75	77	
32	63	54	438	73	8 ₃	
33	60	44	472	70	90	
34	57	35	507	68	6·8 ₃ 96	
35 36 37 38 39	54 50 47 44 41	25 16 8·508 9507 8·508 9497 88	541 576 610 645 679	66 63 61 59 56	6·8403 09 16 22 29	
40	8·508 4838	8·508 9478	1.76714	2°2554	6·8 ₄₃ 6	7:450
41	35	69	749	51	42	
42	32	60	783	49	49	
43	29	51	818	47	55	
44	26	41	853	44	62	
45	22	32	887	42	68	
46	19	23	922	39	75	
47	16	13	957	37	81	
48	13	8·508 9404	1·76991	35	88	
49	10	8·508 9395	1·77026	32	6*8495	
50	8.508 4807	8·508 9385	1.77061	2°2530	6·8501	
51	04	76	096	27	08	
52	8.508 4801	66	131	25	14	
53	8.508 4797	57	166	23	21	
54	94	48	200	20	27	
55	91	38	235	18	34	
56	88	29	270	15	41	
57	85	20	305	13	47	
58	82	10	340	11	54	
59	79	8.508 9301	375	08	60	
60	8.508 4776	8.508 9292	1.77410	2.2509	6.8567	7.440

LATITUDE 67°

Lat.	$\log A'$ diff. $\mathbf{i''} = -0.05$	log B diff. 1"=-0'15	log C diff. 1"=+0.59	$\log D$ $\dim T'' = -0.04$	log E diff. 1"=+o'11	log F diff. 10'= 5'6
67 00 I 2 3	8·508 4776 73 70 66 63	8·508 9292 83 73 64 55	T·77410 445 480 515 550	2·2506 03 2·2501 2·2498 96	- 6 ·8 5 67 • 74 80 87 6 ⋅8 5 94	₹·440
°5	60	46	585	93	6·8600	
6	57	36	620	91	07	
7	54	27	656	89	14	
8	51	18	691	86	20	
9	48	8·508 9208	726	84	27	
10	8.508 4745	8·508 9199	1.77761	2·2481	6·8634	
11	42	90	796	79	40	
12	39	81	831	76	47	
13	36	72	867	74	54	
14	33	62	902	71	60	
15 16 17 18	30 26 23 20	53 44 35 26 16	937 1·77973 1·78008 043 079	69 66 64 61 59	67 74 80 87 6 ·8694	
20	8·508 4714	8·508 9107	1·78114	2°2456	6·8700	7°4 29
21	11	8·508 9098	149	54	07	
22	08	89	185	51	14	
23	05	80	220	49	20	
24	8·508 4702	71	256	46	27	
25	8·508 4699	62	291	44	34	
26	96	52	327	41	41	
27	• 93	43	362	39	47	
28	90	34	398	36	54	
29	87	25	433	34	61	
30	8·508 4684	8·508 9016	1·78469	2°2431	6·8768	
31	81	8·508 9007	505	29	74	
32	78	8·508 8998	540	26	81	
33	75	88	576	24	88	
34	72	79	612	21	6·8795	
35 36 37 38 39	68 65 62 59 56	70 61 52 43 34	647 683 719 755 790	19 16 14 11	6.8802 08 15 22 29	
40	8.508 4653	8·508 8925	1·78826	2·2406	6·8835	7:418
41	50	16	862	03	42	
42	47	8·508 8907	898	2·2401	49	
43	44	8·508 8898	934	2 ·2398	56	
44	41	89	1·78970	96	63	
45	38	80	1°79006	93	70	
46	35	71	042	91	76	
47	32	62	078	88	83	
48	29	53	114	86	90	
49	26	44	150	83	6·8897	
50 51 52 53 54	8·508 4623 20 17 14	8·508 8834 25 16 8·508 8807 8·508 8798	1°79186 222 258 294 .330	2·2380 78 75 73 70	6·8904 10 17 24 31	
55	08	89	366	67	38	
56	05	80	402	65	45	
57	8*508 4602	71	438	62	52	
58	8*508 4599	62	474	60	59	
59	96	54	511	57	65	
60	8.508 4593	8.508 8745	1.79547	2.2354	6.8972	7,406

LATITUDE 68°

Lat.	$\log A'$ diff. $\mathbf{r}'' = - \circ \circ \circ \circ$	$\log B$ $diff. i'' = -o^*i5$	$\log C$ diff. $\mathbf{r}'' = + \circ \cdot 62$	$\log D$ $diff. $	$\log E$ $\dim E + o \cdot 12$	$ \log F $ diff. 10' = -5'9
68 00 I 2 3 4	8·508 4593 90 87 84 81	8·508 8745 36 27 18	ī·79547 583 620 656 692	2·2354 52 49 47 44	6·8972 79 86 6·8993 6·9000	₹.406
05	78	8·508 8700	728	41	07	
6	76	8·508 8691	765	39	14	
7	73	82	801	36	21	
8	70	73	838	33	28	
9	67	64	874	31	35	
10	8·508 4564	8·508 8656	1°79911	2°2328	6°9042	,
11	61	47	947	26	48	
12	58	38	1°79984	23	55	
13	55	29	1°80020	20	62	
14	52	20	. °57	18	69	
15 16 17 18	49 46 43 40 37	8·508 8602 8·508 8593 84 75	093 130 166 203 240	15 12 10 07 04	76 83 90 6*9097 6*9104	
20	8·508 4534	8·508 8566	1.80276	2°2302	6.9111	7:395
21	31	58	313	2°2299	18	
22	28	49	350	96	25	
23	25	40	387	94	32	
24	22	31	423	91	39	
25	19	22	460	88	46	
26	16	13	497	85	53	
27	13	8·508 8505	534	83	60	
28	10	8·508 8496	571	80	67	
29	07	87	608	77	74	
30	8·508 4504	8·508 8478	1·80645	2 ² 275	6·9181	
31	8·508 4501	69	682	72	88	
32	8·508 4499	60	719	69	6·9195	
33	96	52	756	67	6·9203	
34	93	43	793	64	10	
35	90	34	830	• 61	17	
36	87	25	867	58	24	
37	84	17	904	56	31	
38	81	8*508 8408	941	53	38	
39	78	8*508 8399	1·80978	50	45	
40	8·508 4475	8·508 8390	1·81015	2°2248	6·9252	7:383
41	72	82	052	45	59	
42	70	73	089	42	66	
43	67	64	127	39	73	
44	64	56	164	36	80	
45	61	47	201	34	88	
46	58	38	239	31	6·9 <i>2</i> 9 5	
47	55	30	276	28	6·9302	
48	52	21	313	26	09	
49	49	12	350	23	16	
50	8·508 4446	8·508 8303	1.81388	2°2220	6·9323	
51	43	8·508 8295	425	17	30	
52	40	86	463	14	37	
53	38	77	500	12	45	
54	35	68	538	09	52	
. 55	32	60	575	06	. 59	
56	29	51	613	03	66	
57	26	43	650	2·2201	73	
58	23	34	688	2·2198	80	
59	20	25	726	95	88	
60	8.508 4417	8.508 8217	1.81763	2.5165	6.9395	7.371

LATITUDE 69°

Lat.	$\log A'$ $\text{diff. } \mathbf{1''} = -0.05$	log B diff. 1" = -0'14	$\log C$ $\dim C = +0.64$	$\log I)$ $diff. x'' = - o'o5$	$ \begin{array}{c} \log E \\ \dim F & \text{o'12} \end{array} $	$\log F$ diff. $ro' = -6$
o / 69 00 I 2	8·508 4417 14 12	8·508 8217 08 8·508 8200	ī·81763 801 838	2°2192 89	6·9395 6·9402	= 7·371
3 4	09 06	8·508 8191 82	876 914	8 7 84 81	09 16 24	
c5 6 7 8 9	8·508 4400 8·508 4397 94 92	74 65 57 48 39	952 1·81989 1·82027 065 103	78 75 7 ² 70 67	31 38 45 52 60	
10	8·508 4389	8·508 8131	1.82141	2°2164	6°9467	
11	86	22	179	61	74	
12	83	14	217	58	82	
13	80	8·508 8105	255	55	89	
14	77	8·508 8096	293	53	6°9496	
15 16 17 18	74 71 69 66 63	88 79 71 62 54	330 369 407 445 483	50 47 44 41 38	6·9503 11 18 25 32	
20	8·508 4360	8·508 8045	1·82521	2·2136	6·9540	7*358
21	57	37	559	33	47	
22	55	28	597	30	54	
23	52	20	636	27	62	
24	49	11	674	24	69	
25	46	8·508 8003	712	21	76	
26	43	8·508 7994	750	18	84	
27	40	86	789	15	91	
28	37	77	827	12	6·9598	
29	35	69	865	10	6·9606	
. 30	8·508 4332	8·508 7960	1·82904	2·2107	6°9613	
31	29	52	942	04	20	
32	26	43	1·82981	2·2101	28	
33	23	35	1·83019	2·2098	35	
34	21	26	058	95	42	
35	18	18	096	92	50	
36	15	09	135	89	57	
37	12	8·508 7901	173	86	65	
38	09	8·508 7893	212	83	72	
39	06	84	250	80	79	
40	8.508 4304	8·508 7876	1·83289	2·2078	6·9687	7.346
41	8.508 4301	67	328	75	6·9694	
42	8.508 4298	59	366	72	6·9702	
43	95	51	405	69	09	
44	93	42	444	66	16	
45	90	34	. 483	63	24	
46	87	26	521	60	31	
47	84	17	560	57	39	
48	81	09	599	54	46	
49	79	8·508 7801	638	51	54	
50	8·508 4276	8·508 7792	1.83677	2·2048	6·9761	
51	73	84	716	45	69	
52	70	75	755	42	76	
53	67	67	794	39	84	
54	65	59	833	36	91	
55 56 57 58 ·	62 59 56 54 51	50 42 34 25 17	872 911 950 1*83989 1*84028	33 30 27 24 21	6°9799 6°9806 14 21 29	
60	8.508 4248	8.508 7709	1.84068	2.5018	6•9836	7.333

COAST AND GEODETIC SURVEY.

LATITUDE 70°

Lat.	log A' diff. 1"=-0'04	$ \log B $ diff. $\mathbf{1''} = -0.14$	$ \log C $ diff. $x'' = + \circ 67$	$\log D$ diff. $\mathbf{r}'' = -\circ \circ 5$	$\log E$ $\dim F = + \circ \iota_3$	$\log F$ diff. $10' = -6$
° / 70 00 1 2 3 4	8·508 4248 45 43 40 37	8·508 7709 8·508 7701 8·508 7692 84 76	ī·84068 107 146 185 225	2·2018 15 12 09 06	¯6·9836 44 51 59 66	₹:333
05	34	68	264	03	74	
6	32	59	303	2·2000	81	
7	29	51	343	2·1997	89	
8	26	43	382	94	6·9896	
9	23	35	421	91	6·9904	
10 11 12 13	8·508 4221 18 15 12 10	8·508 7626 18 10 8·508 7602 8·508 7594	1·84461 500 540 579 619	2·1988 85 82 79 76	6·9912 19 27 34 42	
15 16 17 18	07 04 8·508 4201 8·508 4199 96	86 78 69 61 52	658 698 738 778 817	73 70 66 63 60	50 57 65 73 80	
20	8·508 4193	8·508 7544	1·84857	2·1957	6·9988	7:320
21	90	36	897	54	6·9995	
22	88	28	937	51	7·0003	
23	85	20	1·84976	48	11	
24	82	12	1·85016	45	18	
25	. 80	8·508 7504	056	42	26	
26	77	8·508 7495	096	39	34	
27	74	87	136	36	41	
28	71	79	176	33	49	
29	69	71	216	29	57	
30	8·508 4166	8·508 7462	1·85256	2°1926	7·0064	
31	63	54	296	23	72	
32	60	46	336	20	80	
33	58	38	376	17	88	
34	55	30	416	14	7·0095	
35	52	22	456	11	7·0103	
36	50	14	497	08	11	
37	47	8·508 7406	537	04	19	
38	44	8·508 7398	577	2·1901	26	
39	42	90	618	2·1898	34	
40	8·508 4139	\$\cdot 508 7382	1·85658	2·1895	7.0142	7.307
41	36	74	698	92	50	
42	34	66	739	89	57	
43	31	58	779	85	65	
44	28	50	819	82	73	
45 46 47 48 49	26 23 20 18 15	42 34 26 18	860 900 941 1·85981 1·86 ₀₂₂	79 76 73 70 66	81 88 7·0196 7·0204 12	
50	8·508 4112	8·508 7302	1·86063	2·1863	7.0220	
51	10	8·508 7294	103	60	27	
52	07	86	144	57	35	
53	04	77	185	54	43	
54	8·508 4101	69	225	50	51	
55	8·508 4099	61	266	47	59	
56	96	53	307	44	67	
57	93	45	348	41	75	
58	91	38	389	38	82	
59	88	30	430	34	90	
60	8.508 4086	8.508 7222	1.86470	2.1831	7.0298	7.293

LATITUDE 71°

Lat.	$\log A'$ $\operatorname{diff.} \mathbf{i''} = -0^{\circ}04$	$ \log \beta \\ \text{diff. } \mathbf{i''} = -0.13 $	$\log C$ $\operatorname{diff.} x'' = +0.70$	$\log I)$ diff. $I'' = -0.05$	$\log E$ $diff. i'' = +0.13$	$ \log F $ $ \dim F = -7^2 $
71 00	8·508 4086	8·508 7222	T·86470	2·1831	7·0298	7 ·293
1	83	14	511	28	7·0306	
2	80	8·508 7206	552	25	14	
3	78	8·508 7198	593	21	22	
4	75	90	634	18	30	
05 6 7 8 9	72 70 67 64 62	82 74 66 58 50	675 717 758 799 840	15 08 05 2·1802	38 46 54 62 70	
10 11 12 13 14	8·508 4059 57 54 51 49	8·508 7142 34 27 19	1•86881 923 1•86964 1•87005 046	2·1799 95 92 89 86	7.0378 85 7.0393 7.0401	
15 16 17 18	46 43 41 38 36	8·508 7103 8·508 7095 87 79 72	088 129 171 212 254	82 79 76 72 69	17 25 33 41 49	
20	8.508 4033	8·508 7064	1·87295	2·1766	7°0457	7 ·279
21	30	56	337	62	65	
22	28	48	378	59	73	
23	25	40	420	56	82	
24	23	33	462	52	90	
25 26 27 28 29	20 17 15 12	25 17 09 8·508 7002 8·508 6994	503 545 587 629 671	49 46 42 39 36	7·0498 7·0506 14 22 30	
30	8·508 4007	8·508 6986	1.87712	2°1732	7.0538	
31	05	78	754	29	46	
32	8·508 4002	71	796	26	54	
33	8·508 3999	63	838	22	62	
34	97	55	880	19	70	
35 36 37 38 39	94 92 89 86 84	47 40 32 24 16	922 1·87964 1·88006 049 091	16 12 09 06 2·1702	79 87 7:0595 7:0603	
40	8·508 3981	8·508 6908	1.88133	2·1699	7.0619	7·265
41	79	8·508 6901	175	95	27	
42	76	8·508 6893	217	92	36	
43	74	85	260	89	44	
44	71	78	302	85	52	
45	68	70	344	82	60	
46	66	62	387	78	68	
47	63	55	429	75	77	
48	61	47	472	72	85	
49	58	40	514	68	7.0693	
50	8·508 3956	8·508 6832	1·88557	2·1665	7·0701	
51	53	24	599	61	09	
52	51	17	642	58	18	
53	48	09	685	54	26	
54	46	8·508 6802	727	51	34	
55	43	8·508 6794	770	48	42	
56	41	86	813	44	51	
57	38	79	855	41	59	
58	36	71	898	37	67	
59	33	64	941	34	75	
60	8.508 3930	8.508 6756	1.88984	2.1630	7.0784	7.250

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